



钜地半导体
Tudi Semiconductor

Product Specification

TUDI-TPD741

700-mW MONO LOW-VOLTAGE AUDIO POWER AMPLIFIER
WITH DIFFERENTIAL INPUTS

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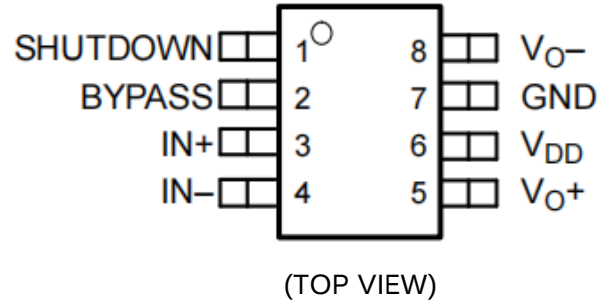
**semiconductor device
manufacturer**

- Design
- research and development
- production
- and sales



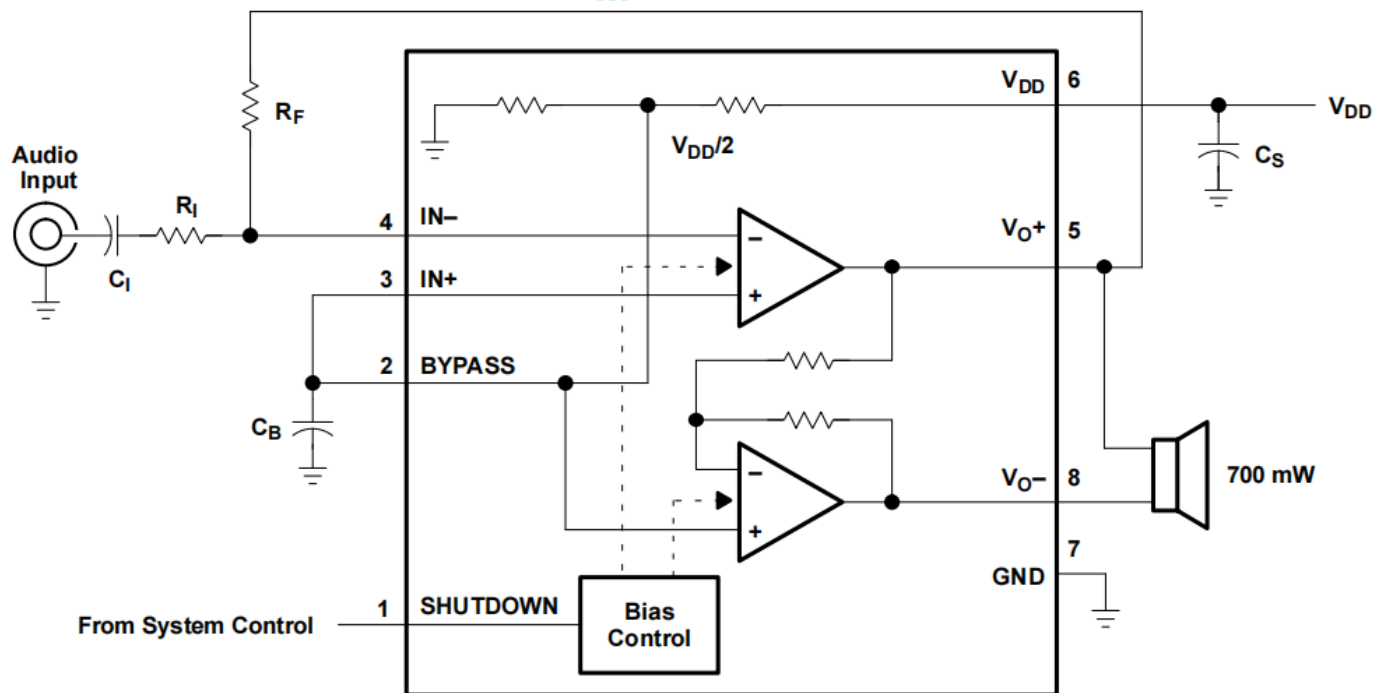
FEATURES

- Fully Specified for 3.3-V and 5-V Operation
- Wide Power Supply Compatibility 2.5V-5.5V
- Output Power for $R_L=8\Omega$
 - 700 mW at $V_{DD}=5V$
 - 250 mW at $V_{DD}=3.3 V$
- Integrated Depop Circuitry
- Thermal and Short-Circuit Protection
- Surface-Mount Packaging
 - SOIC
 - PowerPAD™ MSOP



DESCRIPTION

The TPA741 is a bridge-tied load (BTL) audio power amplifier developed especially for low-voltage applications where internal speakers are required. Operating with a 3.3-V supply, the TPA741 can deliver 250-mW of continuous power into a BTL 8- Ω load at less than 0.6% THD+N throughout voice band frequencies. Although this device is characterized out to 20 kHz, its operation is optimized for narrower band applications such as wireless communications. The BTL configuration eliminates the need for external coupling capacitors on the output in most applications, which is particularly important for small battery-powered equipment. This device features a shutdown mode for power-sensitive applications with a supply current of 7 μA during shutdown. The TPA741 is available in an 8-pin SOIC surface-mount package and the surface-mount PowerPAD™ MSOP, which reduces board space by 50% and height by 40%.



AVAILABLE OPTIONS

T _A	PACKAGED DEVICES		MSOP SYMBOLIZATION
	SMALL OUTLINE ⁽¹⁾ (D)	MSOP ⁽²⁾ (DGN)	
-40°C to 85°C	TPA741D	TPA741DGN	AJD

- (1) In the D package, the maximum output power is thermally limited to 350 mW; 700-mW peaks can be driven, as long as the RMS value is less than 350 mW.
- (2) The D and DGN packages are available taped and reeled. To order a taped and reeled part, add the suffix R to the part number (e.g., TPA741DR).

Terminal Functions

TERMINAL NAME	NO.	I/O	DESCRIPTION
BYPASS	2	I	BYPASS is the tap to the voltage divider for internal mid-supply bias. This terminal should be connected to a 0.1-μF to 2.2-μF capacitor when used as an audio amplifier.
GND	7		GND is the ground connection.
IN-	4	I	IN- is the inverting input. IN- is typically used as the audio input terminal.
IN+	3	I	IN+ is the noninverting input. IN+ is typically tied to the BYPASS terminal for SE operations.
SHUTDOWN	1	I	SHUTDOWN places the entire device in shutdown mode when held high.
V _{DD}	6		V _{DD} is the supply voltage terminal.
V _{O+}	5	O	V _{O+} is the positive BTL output.
V _{O-}	8	O	V _{O-} is the negative BTL output.



ABSOLUTE MAXIMUM RATINGS

over operating free-air temperature range (unless otherwise noted)⁽¹⁾

	UNIT
V _{DD} Supply voltage	6 V
V _I Input voltage	−0.3 V to V _{DD} +0.3 V
Continuous total power dissipation	Internally limited (see Dissipation Rating Table)
T _A Operating free-air temperature range	−40°C to 85°C
T _J Operating junction temperature range	−40°C to 150°C
T _{stg} Storage temperature range	−65°C to 150°C
Lead temperature 1,6 mm (1/16 inch) from case for 10 seconds	260°C

- (1) Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

DISSIPATION RATING TABLE

PACKAGE	T _A ≤ 25°C	DERATING FACTOR	T _A = 70°C	T _A = 85°C
D	725 mW	5.8 mW/°C	464 mW	377 mW
DGN	2.14 W ⁽¹⁾	17.1 mW/°C	1.37 W	1.11 W

- (1) See the Texas Instruments document, *PowerPAD Thermally Enhanced Package Application Report* (SLMA002), for more information on the PowerPAD package. The thermal data was measured on a PCB layout based on the information in the section entitled *Texas Instruments Recommended Board for PowerPAD* of that document.

RECOMMENDED OPERATING CONDITIONS

	MIN	MAX	UNIT
V _{DD} Supply voltage,	2.5	5.5	V
V _{IH} High-level voltage (SHUTDOWN)	0.9V _{DD}		V
V _{IL} Low-level voltage (SHUTDOWN)		0.1V _{DD}	V
T _A Operating free-air temperature	−40	85	°C

ELECTRICAL CHARACTERISTICS

at specified free-air temperature, V_{DD} = 3.3 V, T_A = 25°C (unless otherwise noted)

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
V _{OS} Output offset voltage (measured differentially)	SHUTDOWN = 0 V, R _L = 8 Ω, R _F = 10 kΩ			20	mV
PSRR Power supply rejection ratio	V _{DD} = 3.2 V to 3.4 V		85		dB
I _{DD} Supply current	SHUTDOWN = 0 V, R _F = 10 kΩ		1.35	2.5	mA
I _{DD(SD)} Supply current, shutdown mode (see Figure 6)	SHUTDOWN = V _{DD} , R _F = 10 kΩ		7	50	μA
I _{IH}	SHUTDOWN, V _{DD} = 3.3 V, V _I = 3.3 V			1	μA
I _{IL}	SHUTDOWN, V _{DD} = 3.3 V, V _I = 0 V			1	μA



OPERATING CONDITIONS

$V_{DD} = 3.3\text{ V}$, $T_A = 25^\circ\text{C}$, $R_L = 8\ \Omega$

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
P_O Output power, See ⁽¹⁾	THD = 0.5%, See Figure 9		250		mW
THD + N Total harmonic distortion plus noise	$P_O = 250\text{ mW}$, $f = 200\text{ Hz to }4\text{ kHz}$, See Figure 7		0.55%		
B_{OM} Maximum output power bandwidth	$A_V = -2\text{ V/V}$, THD = 2%, See Figure 7		20		kHz
B_1 Unity-gain bandwidth	Open loop, See Figure 15		1.4		MHz
k_{SVR} Supply ripple rejection ratio	$f = 1\text{ kHz}$, $C_B = 1\ \mu\text{F}$, See Figure 2		79		dB
V_n Noise output voltage	$A_V = -1\text{ V/V}$, $C_B = 0.1\ \mu\text{F}$, See Figure 19		17		$\mu\text{V(rms)}$

(1) Output power is measured at the output terminals of the device at $f = 1\text{ kHz}$.

ELECTRICAL CHARACTERISTICS

at specified free-air temperature, $V_{DD} = 5\text{ V}$, $T_A = 25^\circ\text{C}$ (unless otherwise noted)

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
$ V_{OS} $ Output offset voltage (measured differentially)	SHUTDOWN = 0 V, $R_L = 8\ \Omega$, $R_F = 10\text{ k}\Omega$			20	mV
PSRR Power supply rejection ratio	$V_{DD} = 4.9\text{ V to }5.1\text{ V}$		78		dB
I_{DD} Supply current	SHUTDOWN = 0 V, $R_F = 10\text{ k}\Omega$		1.45	2.5	mA
$I_{DD(SD)}$ Supply current, shutdown mode (see Figure 4)	SHUTDOWN = V_{DD} , $R_F = 10\text{ k}\Omega$		50	100	μA
$ I_{IH} $	SHUTDOWN, $V_{DD} = 5.5\text{ V}$, $V_i = V_{DD}$			1	μA
$ I_{IL} $	SHUTDOWN, $V_{DD} = 5.5\text{ V}$, $V_i = 0\text{ V}$			1	μA

OPERATING CHARACTERISTICS

$V_{DD} = 5\text{ V}$, $T_A = 25^\circ\text{C}$, $R_L = 8\ \Omega$

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
P_O Output power	THD = 0.5%, See Figure 13		700 ⁽¹⁾		mW
THD + N Total harmonic distortion plus noise	$P_O = 250\text{ mW}$, $f = 200\text{ Hz to }4\text{ kHz}$, See Figure 11		0.5%		
B_{OM} Maximum output power bandwidth	$A_V = -2\text{ V/V}$, THD = 2%, See Figure 11		20		kHz
B_1 Unity-gain bandwidth	Open loop, See Figure 16		1.4		MHz
k_{SVR} Supply ripple rejection ratio	$f = 1\text{ kHz}$, $C_B = 1\ \mu\text{F}$, See Figure 2		80		dB
V_n Noise output voltage	$A_V = -1\text{ V/V}$, $C_B = 0.1\ \mu\text{F}$, See Figure 20		17		$\mu\text{V(rms)}$

(1) The DGN package, properly mounted, can conduct 700-mW RMS power continuously. The D package can only conduct 350-mW RMS power continuously with peaks to 700 mW.



PARAMETER MEASUREMENT INFORMATION

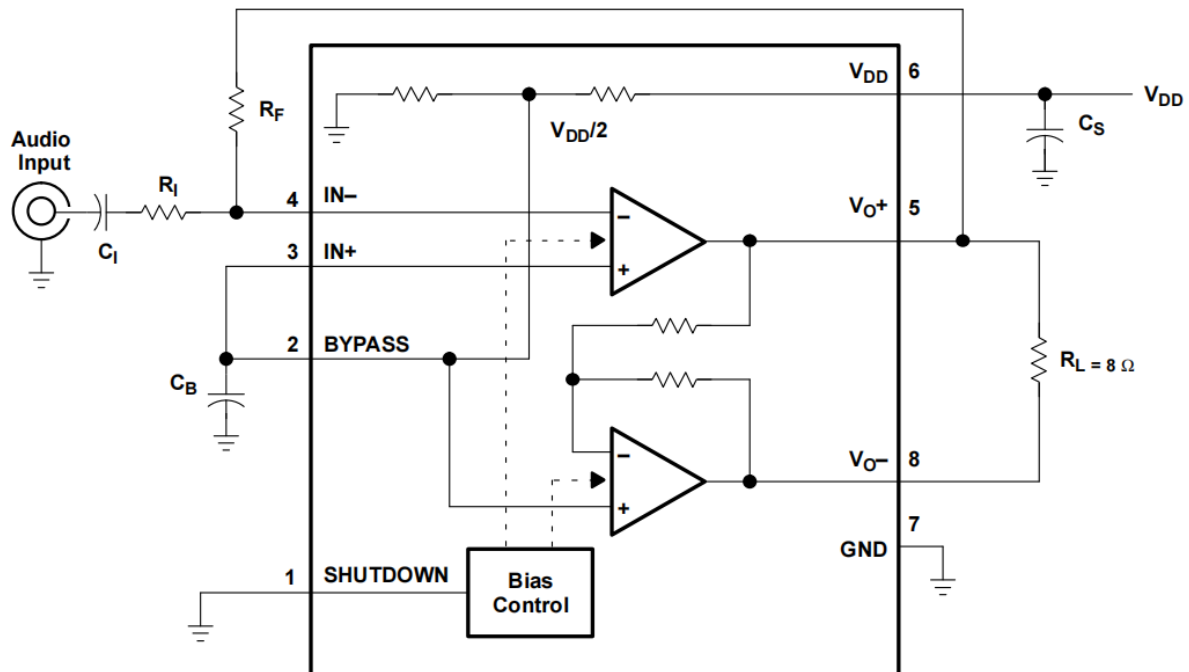


Figure 1. BTL Mode Test Circuit

TYPICAL CHARACTERISTICS

Table of Graphs

			FIGURE
k_{SVR}	Supply ripple rejection ratio	vs Frequency	2
I_{DD}	Supply current	vs Supply voltage	3, 4
P_O	Output power	vs Supply voltage	5
		vs Load resistance	6
THD+N	Total harmonic distortion plus noise	vs Frequency	7, 8, 11, 12
		vs Output power	9, 10, 13, 14
	Open-loop gain and phase	vs Frequency	15, 16
	Closed-loop gain and phase	vs Frequency	17, 18
V_n	Output noise voltage	vs Frequency	19, 20
P_D	Power dissipation	vs Output power	21, 22



APPLICATION INFORMATION

BRIDGE-TIED LOAD

Figure 23 shows a linear audio power amplifier (APA) in a BTL configuration. The TPA741 BTL amplifier consists of two linear amplifiers driving both ends of the load. There are several potential benefits to this differential drive configuration, but initially consider power to the load. The differential drive to the speaker means that as one side is slewing up, the other side is slewing down, and vice versa. This, in effect, doubles the voltage swing on the load as compared to a ground referenced load. Plugging $2 \times V_{O(PP)}$ into the power equation, where voltage is squared, yields $4 \times$ the output power from the same supply rail and load impedance (see Equation 1).

$$V_{(rms)} = \frac{V_{O(PP)}}{2\sqrt{2}}$$

$$Power = \frac{V_{(rms)}^2}{R_L} \quad (1)$$

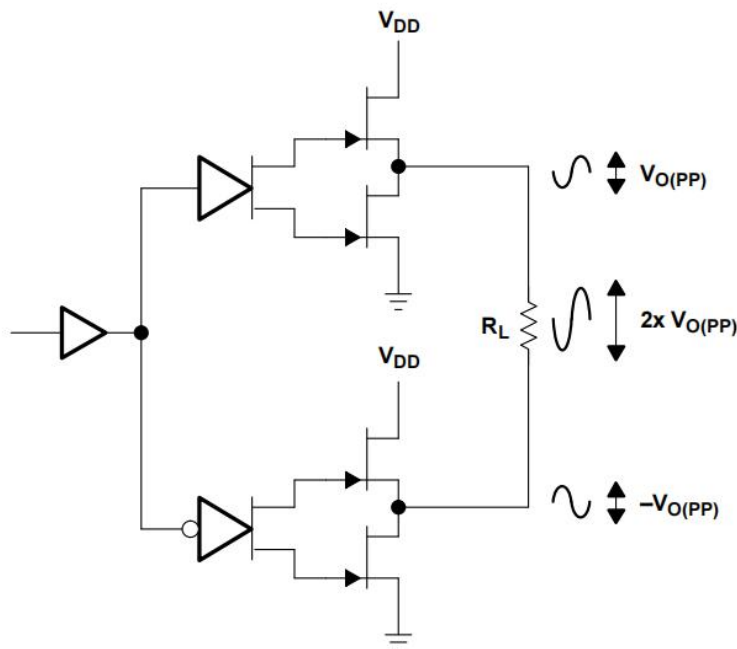


Figure 23. Bridge-Tied Load Configuration

In a typical portable handheld equipment sound channel operating at 3.3 V, bridging raises the power into an 8-Ω speaker from a singled-ended (SE, ground reference) limit of 62.5 mW to 250 mW. In sound power that is a 6-dB improvement, which is loudness that can be heard. In addition to increased power, there are frequency response concerns. Consider the single-supply, SE configuration shown in Figure 24. A coupling capacitor is required to block the dc offset voltage from reaching the load. These capacitors can be quite large (approximately 33 μF to 1000 μF), so they tend to be expensive, heavy, occupy valuable PCB area, and have the additional drawback of limiting low-frequency performance of the system. This frequency-limiting effect is due to the high-pass filter network created with the speaker impedance and the coupling capacitance and is calculated with Equation 2.

$$f_c = \frac{1}{2\pi R_L C_C} \quad (2)$$

For example, a 68-μF capacitor with an 8-Ω speaker would attenuate low frequencies below 293 Hz. The BTL configuration cancels the dc offsets, which eliminates the need for the blocking capacitors. Low-frequency performance is then limited only by the input network and speaker response. Cost and PCB space are also minimized by eliminating the bulky coupling capacitor.



APPLICATION INFORMATION (continued)

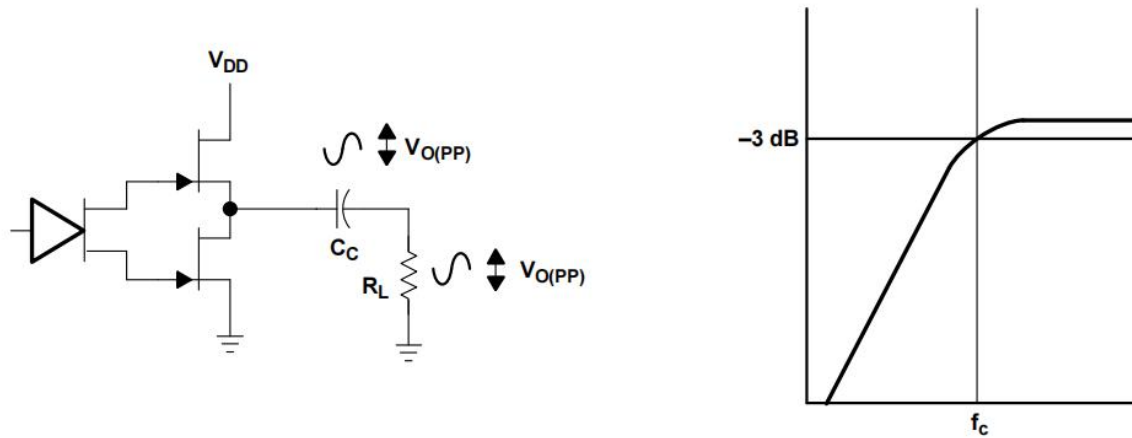


Figure 24. Single-Ended Configuration and Frequency Response

Increasing power to the load does carry a penalty of increased internal power dissipation. The increased dissipation is understandable considering that the BTL configuration produces $4\times$ the output power of a SE configuration. Internal dissipation versus output power is discussed further in the *thermal considerations* section.

BTL AMPLIFIER EFFICIENCY

Linear amplifiers are notoriously inefficient. The primary cause of these inefficiencies is voltage drop across the output stage transistors. There are two components of the internal voltage drop. One is the headroom or dc voltage drop that varies inversely to output power. The second component is due to the sine-wave nature of the output. The total voltage drop can be calculated by subtracting the RMS value of the output voltage from V_{DD} . The internal voltage drop multiplied by the RMS value of the supply current, $I_{DD(RMS)}$, determines the internal power dissipation of the amplifier.

An easy-to-use equation to calculate efficiency starts out being equal to the ratio of power from the power supply to the power delivered to the load. To accurately calculate the RMS values of power in the load and in the amplifier, the current and voltage waveform shapes must first be understood (see Figure 25).

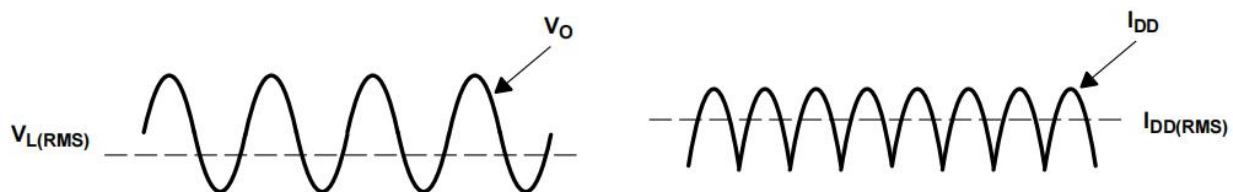


Figure 25. Voltage and Current Waveforms for BTL Amplifiers

Although the voltages and currents for SE and BTL are sinusoidal in the load, currents from the supply are different between SE and BTL configurations. In an SE application, the current waveform is a half-wave rectified shape, whereas in BTL it is a full-wave rectified waveform. This means RMS conversion factors are different. Keep in mind that for most of the waveform both the push and pull transistors are not on at the same time, which supports the fact that each amplifier in the BTL device only draws current from the supply for half the waveform. The following equations are the basis for calculating amplifier efficiency.



APPLICATION INFORMATION (continued)

$$\text{Efficiency} = \frac{P_L}{P_{\text{SUP}}}$$

where

$$P_L = \frac{V_{L(\text{RMS})}^2}{R_L} = \frac{V_p^2}{2R_L}$$

$$V_{L(\text{RMS})} = \frac{V_P}{\sqrt{2}}$$

$$P_{\text{SUP}} = V_{\text{DD}} I_{\text{DD}(\text{RMS})} = \frac{V_{\text{DD}}^2 V_P}{\pi R_L}$$

$$I_{\text{DD}(\text{RMS})} = \frac{2V_P}{\pi R_L}$$

(3)

$$\text{Efficiency of a BTL configuration} = \frac{\pi V_P}{4V_{\text{DD}}} = \frac{\pi (2 P_L R_L)^{1/2}}{4V_{\text{DD}}}$$

(4)

Table 1 employs Equation 4 to calculate efficiencies for three different output power levels. The efficiency of the amplifier is quite low for lower power levels and rises sharply as power to the load is increased, resulting in a nearly flat internal power dissipation over the normal operating range. The internal dissipation at full output power is less than in the half power range. Calculating the efficiency for a specific system is the key to proper power supply design.

Table 1. Efficiency vs Output Power in 3.3-V, 8-Ω, BTL Systems

OUTPUT POWER (W)	EFFICIENCY (%)	PEAK VOLTAGE (V)	INTERNAL DISSIPATION (W)
0.125	33.6	1.41	0.26
0.25	47.6	2.00	0.29
0.375	58.3	2.45 ⁽¹⁾	0.28

(1) High-peak voltage values cause the THD to increase.

A final point to remember about linear amplifiers (either SE or BTL) is how to manipulate the terms in the efficiency equation to utmost advantage when possible. In Equation 4, V_{DD} is in the denominator. This indicates that as V_{DD} goes down, efficiency goes up.



APPLICATION SCHEMATICS

Figure 26 is a schematic diagram of a typical handheld audio application circuit, configured for a gain of -10 V/V.

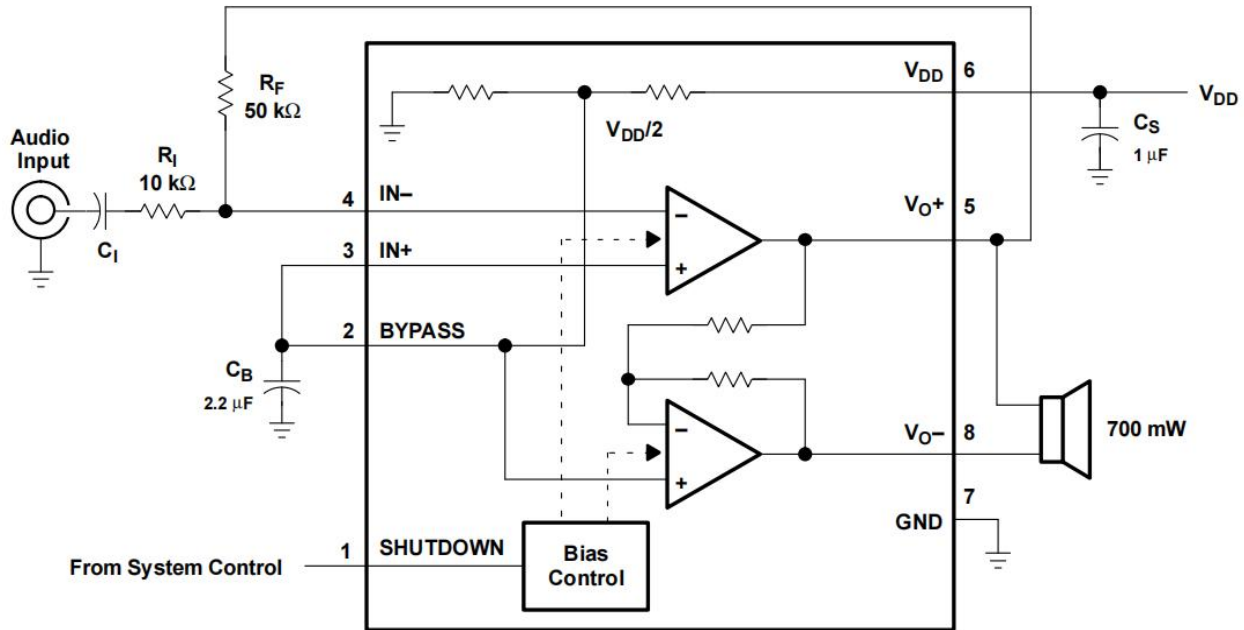


Figure 26. TPA741 Application Circuit

Figure 27 is a schematic diagram of a typical handheld audio application circuit, configured for a gain of -10 V/V with a differential input.

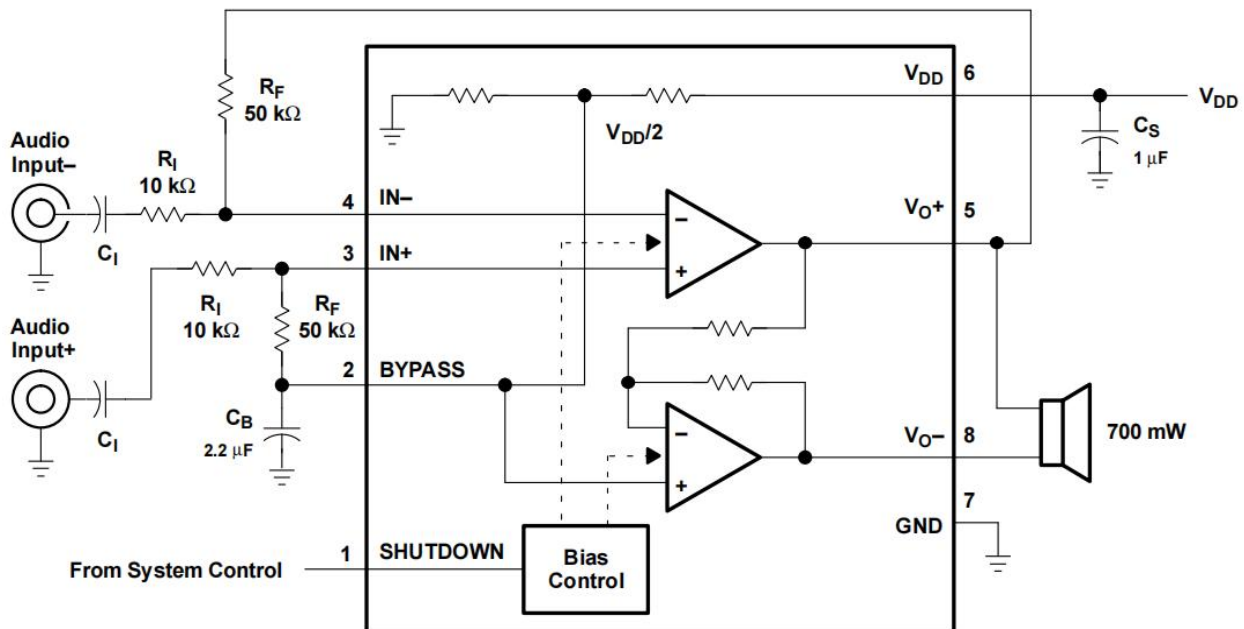


Figure 27. TPA741 Application Circuit With Differential Input

It is important to note that using the additional R_F resistor connected between $IN+$ and $BYPASS$ will cause $V_{DD}/2$ to shift slightly, which could influence the THD+N performance of the amplifier. Although an additional external operational amplifier could be used to buffer $BYPASS$ from R_F , tests in the laboratory have shown that the THD+N performance is only minimally affected by operating in the fully differential mode as shown in Figure 27. The following sections discuss the selection of the components used in Figure 26 and Figure 27.



COMPONENT SELECTION

Gain-Setting Resistors, R_F and R_I

The gain for each audio input of the TPA741 is set by resistors R_F and R_I according to Equation 5 for BTL mode.

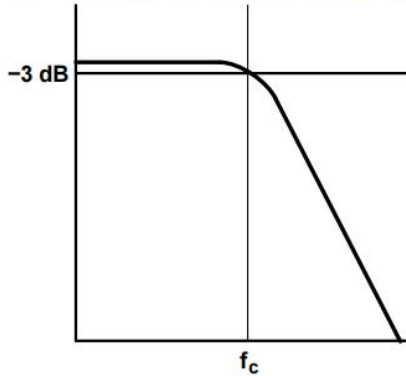
$$\text{BTL gain} = -2 \left(\frac{R_F}{R_I} \right) \quad (5)$$

BTL mode operation brings about the factor 2 in the gain equation due to the inverting amplifier mirroring the voltage swing across the load. Given that the TPA741 is an MOS amplifier, the input impedance is high; consequently, input leakage currents are not generally a concern, although noise in the circuit increases as the value of R_F increases. In addition, a certain range of R_F values is required for proper start-up operation of the amplifier. Taken together, it is recommended that the effective impedance seen by the inverting node of the amplifier be set between 5 k Ω and 20 k Ω . The effective impedance is calculated in Equation 6.

$$\text{Effective impedance} = \frac{R_F R_I}{R_F + R_I} \quad (6)$$

As an example, consider an input resistance of 10 k Ω and a feedback resistor of 50 k Ω . The BTL gain of the amplifier would be -10 V/V and the effective impedance at the inverting terminal would be 8.3 k Ω , which is well within the recommended range.

For high-performance applications, metal film resistors are recommended because they tend to have lower noise levels than carbon resistors. For values of R_F above 50 k Ω , the amplifier tends to become unstable due to a pole formed from R_F and the inherent input capacitance of the MOS input structure. For this reason, a small compensation capacitor of approximately 5 pF should be placed in parallel with R_F when R_F is greater than 50 k Ω . This, in effect, creates a low-pass filter network with the cutoff frequency defined in Equation 7.

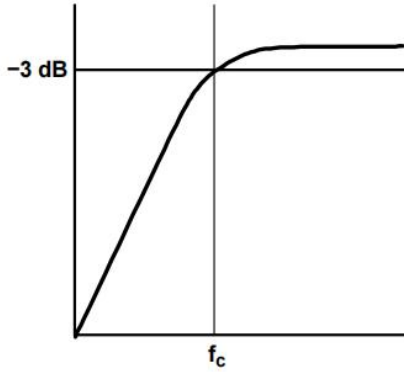


$$f_c = \frac{1}{2\pi R_F C_F} \quad (7)$$

For example, if R_F is 100 k Ω and C_F is 5 pF, then f_c is 318 kHz, which is well outside of the audio range.

Input Capacitor, C_I

In the typical application an input capacitor, C_I , is required to allow the amplifier to bias the input signal to the proper dc level for optimum operation. In this case, C_I and R_I form a high-pass filter with the corner frequency determined in Equation 8.



$$f_c = \frac{1}{2\pi R_I C_I}$$

(8)

The value of C_I is important to consider as it directly affects the bass (low-frequency) performance of the circuit. Consider the example where R_I is 10 k Ω and the specification calls for a flat bass response down to 40 Hz. Equation 8 is reconfigured as Equation 9.

$$C_I = \frac{1}{2\pi R_I f_c}$$

(9)

In this example, C_I is 0.4 μ F, so one would likely choose a value in the range of 0.47 μ F to 1 μ F. A further consideration for this capacitor is the leakage path from the input source through the input network (R_I , C_I) and the feedback resistor (R_F) to the load. This leakage current creates a dc offset voltage at the input to the amplifier that reduces useful headroom, especially in high-gain applications. For this reason, a low-leakage tantalum or ceramic capacitor is the best choice. When polarized capacitors are used, the positive side of the capacitor should face the amplifier input in most applications as the dc level there is held at $V_{DD}/2$, which is likely higher than the source dc level. It is important to confirm the capacitor polarity in the application.

Power Supply Decoupling, C_S

The TPA741 is a high-performance CMOS audio amplifier that requires adequate power supply decoupling to ensure the output total harmonic distortion (THD) is as low as possible. Power supply decoupling also prevents oscillations for long lead lengths between the amplifier and the speaker. The optimum decoupling is achieved by using two capacitors of different types that target different types of noise on the power supply leads. For higher frequency transients, spikes, or digital hash on the line, a good low equivalent-series-resistance (ESR) ceramic capacitor, typically 0.1 μ F, placed as close as possible to the device V_{DD} lead, works best. For filtering lower frequency noise signals, a larger aluminum electrolytic capacitor of 10 μ F or greater, placed near the audio power amplifier is recommended.

Midrail Bypass Capacitor, C_B

The midrail bypass capacitor, C_B , is the most critical capacitor and serves several important functions. During start-up or recovery from shutdown mode, C_B determines the rate at which the amplifier starts up. The second function is to reduce noise produced by the power supply caused by coupling into the output drive signal. This noise is from the midrail generation circuit internal to the amplifier, which appears as degraded PSRR and THD + N. The capacitor is fed from a 250-k Ω source inside the amplifier. To keep the start-up pop as low as possible, the relationship shown in Equation 10 should be maintained. This ensures that the input capacitor is fully charged before the bypass capacitor is fully charged and the amplifier starts up.

$$\frac{10}{(C_B \times 250 \text{ k}\Omega)} \leq \frac{1}{(R_F + R_I) C_I} \quad (10)$$

As an example, consider a circuit where C_B is 2.2 μ F, C_I is 0.47 μ F, R_F is 50 k Ω , and R_I is 10 k Ω . Inserting these values into the Equation 10 we get:

$$18.2 \leq 35.5$$

which satisfies the rule. Bypass capacitor, C_B , values of 0.1- μ F to 2.2- μ F ceramic or tantalum low-ESR capacitors are recommended for the best THD and noise performance.



USING LOW-ESR CAPACITORS

Low-ESR capacitors are recommended throughout this applications section. A real (as opposed to ideal) capacitor can be modeled simply as a resistor in series with an ideal capacitor. The voltage drop across this resistor minimizes the beneficial effects of the capacitor in the circuit. The lower the equivalent value of this resistance, the more the real capacitor behaves like an ideal capacitor.

5-V Versus 3.3-V OPERATION

The TPA741 operates over a supply range of 2.5 V to 5.5 V. This data sheet provides full specifications for 5-V and 3.3-V operation, as these are considered to be the two most common standard voltages. There are no special considerations for 3.3-V versus 5-V operation with respect to supply bypassing, gain setting, or stability. The most important consideration is that of output power. Each amplifier in TPA741 can produce a maximum voltage swing of $V_{DD} - 1$ V. This means, for 3.3-V operation, clipping starts to occur when $V_{O(PP)} = 2.3$ V, as opposed to $V_{O(PP)} = 4$ V for 5-V operation. The reduced voltage swing subsequently reduces maximum output power into an 8- Ω load before distortion becomes significant.

Operation from 3.3-V supplies, as can be shown from the efficiency formula in Equation 4, consumes approximately two-thirds the supply power of operation from 5-V supplies for a given output-power level.

HEADROOM AND THERMAL CONSIDERATIONS

Linear power amplifiers dissipate a significant amount of heat in the package under normal operating conditions. A typical music CD requires 12 dB to 15 dB of dynamic headroom to pass the loudest portions without distortion as compared with the average power output. From the TPA741 data sheet, one can see that when the TPA741 is operating from a 5-V supply into a 8- Ω speaker that 700-mW peaks are available. Converting watts to dB:

$$P_{dB} = 10 \log \frac{P_W}{P_{ref}} = 10 \log \frac{700 \text{ mW}}{1 \text{ W}} = -1.5 \text{ dB}$$

Subtracting the headroom restriction to obtain the average listening level without distortion yields:

$$1.5 \text{ dB} - 15 \text{ dB} = -16.5 \text{ (15-dB headroom)}$$

$$1.5 \text{ dB} - 12 \text{ dB} = -13.5 \text{ (12-dB headroom)}$$

$$1.5 \text{ dB} - 9 \text{ dB} = -10.5 \text{ (9-dB headroom)}$$

$$1.5 \text{ dB} - 6 \text{ dB} = -7.5 \text{ (6-dB headroom)}$$

$$1.5 \text{ dB} - 3 \text{ dB} = -4.5 \text{ (3-dB headroom)}$$

Converting dB back into watts:

$$P_W = 10^{P_{dB}/10} \times P_{ref}$$

$$= 22 \text{ mW (15-dB headroom)}$$

$$= 44 \text{ mW (12-dB headroom)}$$

$$= 88 \text{ mW (9-dB headroom)}$$

$$= 175 \text{ mW (6-dB headroom)}$$

$$= 350 \text{ mW (3-dB headroom)}$$

This is valuable information to consider when attempting to estimate the heat dissipation requirements for the amplifier system. Comparing the absolute worst case, which is 700 mW of continuous power output with 0 dB of headroom, against 12-dB and 15-dB applications drastically affects maximum ambient temperature ratings for the system. Using the power dissipation curves for a 5-V, 8- Ω system, the internal dissipation in the TPA741 and maximum ambient temperatures is shown in Table 2.

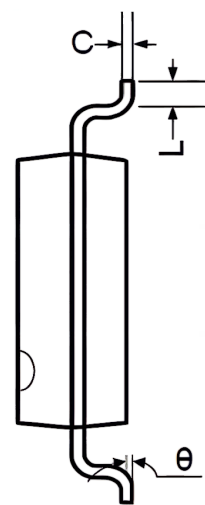
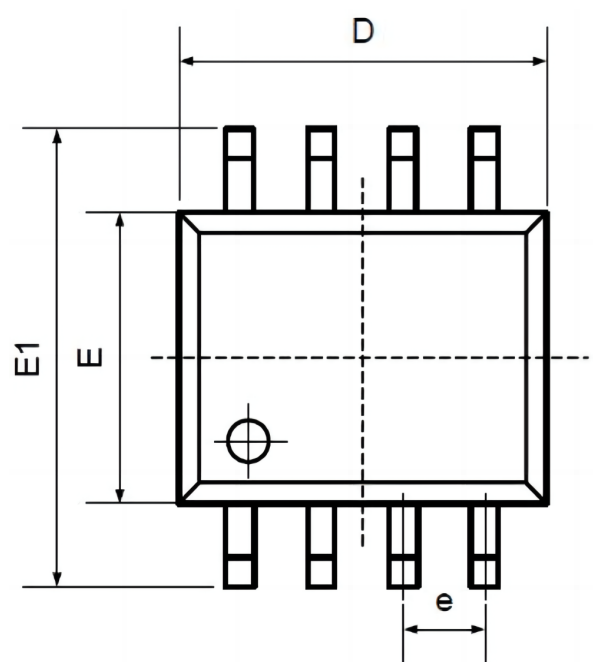


ORDERING INFORMATION

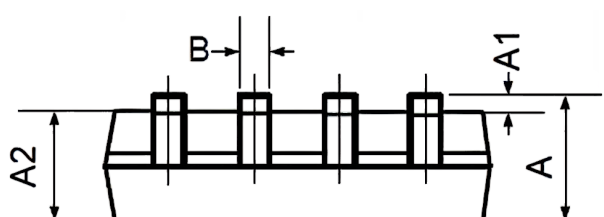
Order Number	Package	Package Quantity	Marking On The park
TPA741DGNR-TUDI	MSOP8	Tape,Reel,2500	AJD
TPA741DR-TUDI	SOP8	Tape,Reel,2500	TPA741



Package SOP8

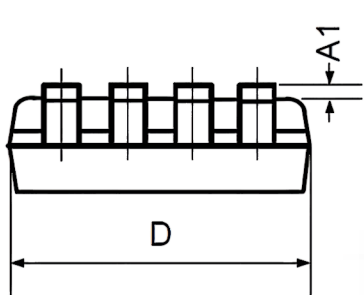
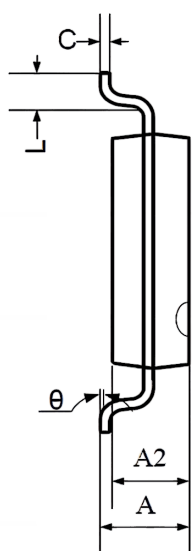
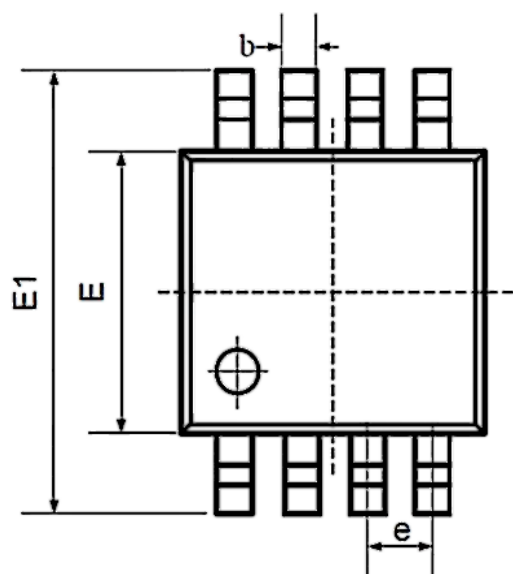


Symbol	Dimensions In Millimeters		Dimensions In Inches	
	Min	Max	Min	Max
A	1.350	1.750	0.053	0.069
A1	0.100	0.250	0.004	0.010
A2	1.350	1.550	0.053	0.061
B	0.330	0.510	0.013	0.020
C	0.190	0.250	0.007	0.010
D	4.780	5.000	0.188	0.197
E	3.800	4.000	0.150	0.157
E1	5.800	6.300	0.228	0.248
e	1.270TYP		0.050TYP	
L	0.400	1.270	0.016	0.050
θ	0°	8°	0°	8°





Package MSOP8



Symbol	Dimensions In Millimeters		Dimensions In Inches	
	Min	Max	Min	Max
A	0.800	1.200	0.031	0.047
A1	0.000	0.200	0.000	0.008
A2	0.760	0.970	0.030	0.038
b	0.30 TYP		0.012 TYP	
C	0.15 TYP		0.006 TYP	
D	2.900	3.100	0.114	0.122
e	0.65 TYP		0.026 TYP	
E	2.900	3.100	0.114	0.122
E1	4.700	5.100	0.185	0.201
L	0.410	0.650	0.016	0.026
θ	0°	6°	0°	6°



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