

## Ultra-Low-EMI, RNS, Mono, Filter-Free, Class-D Audio Amplifier

### Features

- **EEE Function, Greatly reduces EMI over the full bandwidth**
- **Excellent Pop-Click Suppression**
- **RNS (RF-TDD Noise Suppression)**
- 0.008%THD+N (Pout=0.4W, V<sub>DD</sub>=4.2V)
- Filter-Free Class-D Architecture
- Up to 90% Efficiency
- High PSRR (75dB at 217Hz)
- Low Quiescent Current (2.8mA)
- Low Shutdown Current (<0.1μA)
- Power Supply Range: 2.5V~5.5V
- Over-Current Protection
- Over-Temperature Protection
- Small WLCSP 1.25mmX1.185mm-9B Package
- RoHS compliant, lead-free packages

### Applications

- Cellular Phones
- MP3/PMP
- GPS
- Digital Photo Frame

### Typical Application Circuits

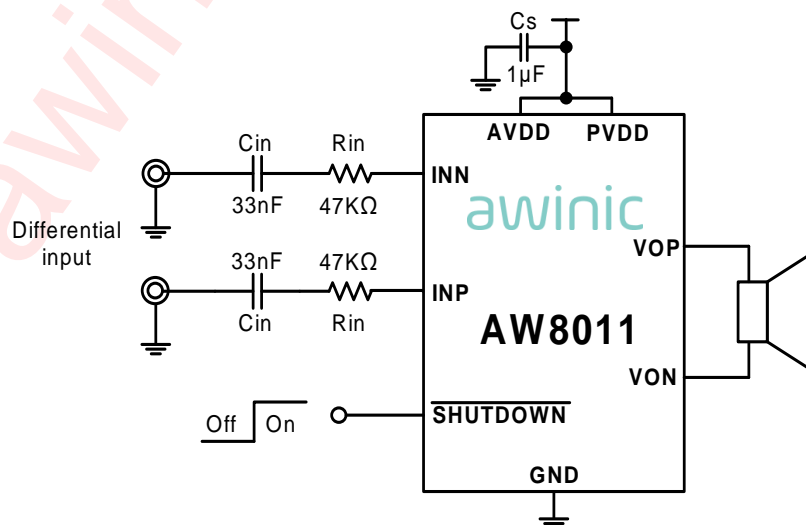


Figure 1 AW8011 Application Schematic With Differential Input

### General Description

The AW8011 is a ultra-low-EMI, RNS, mono, filter-free, Class-D audio amplifier. Unique RNS, which effectively reduces RF energy, attenuate the RF TDD-noise, an acceptable audible level to the customer.

The AW8011 features the EEE (Enhanced Emission Elimination) function which greatly reduces EMI over the full bandwidth. The AW8011 achieves better than 20dB margin under FCC limits with 24 inch of cable.

The filter-free PWM architecture and internal gain setting reduces external components count, board area consumption, system cost and simplifies the design. In addition, The AW8011 offers efficiencies above 90%. The over-current and over-temperature is prepared inside of the device.

The AW8011 is available in an ultra small WLCSP 1.25mmX1.185mmX0.582mm-9B package. The AW8011 is specified over the industrial temperature range of -40°C to +85°C.

## Pin Configuration And Top Mark

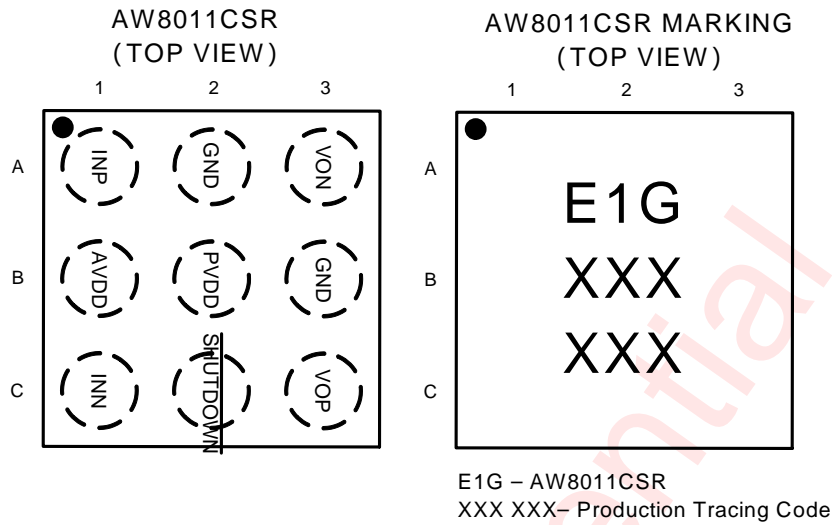


Figure 2 Pin Configuration and Top Mark of AW8011

## Pin Definition

No.	NAME	DESCRIPTION
A1	INP	Positive audio input
A2	GND	Ground
A3	VON	Negative audio output
B1	AVDD	Power Supply
B2	PVDD	Power Supply
B3	GND	Ground
C1	INN	Negative audio input
C2	<u>SHUTDOWN</u>	Shutdown pin
C3	VOP	Positive audio output

## Functional Block Diagram

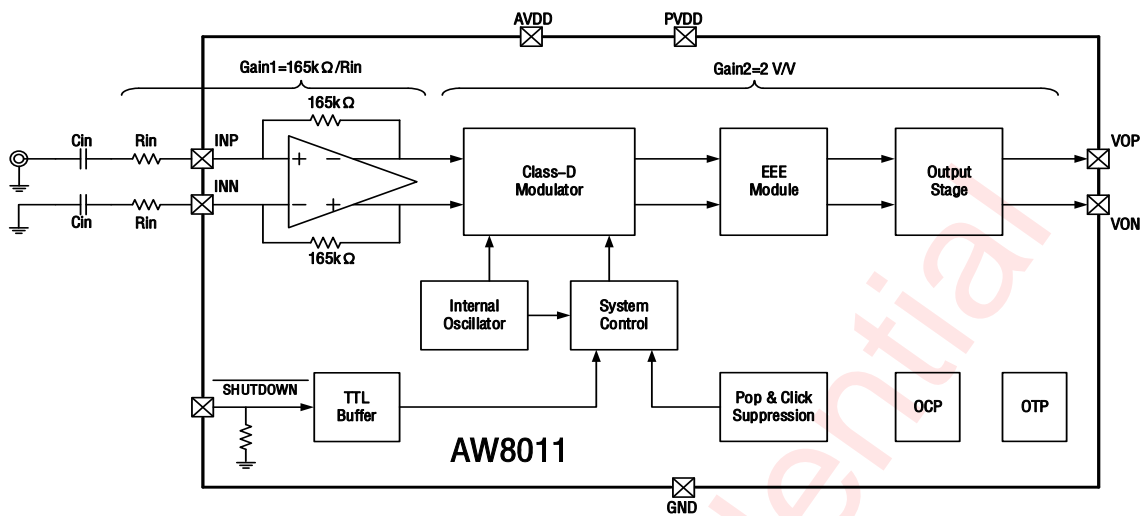


Figure 3 Functional Block Diagram of AW8011

## Typical Application Circuits

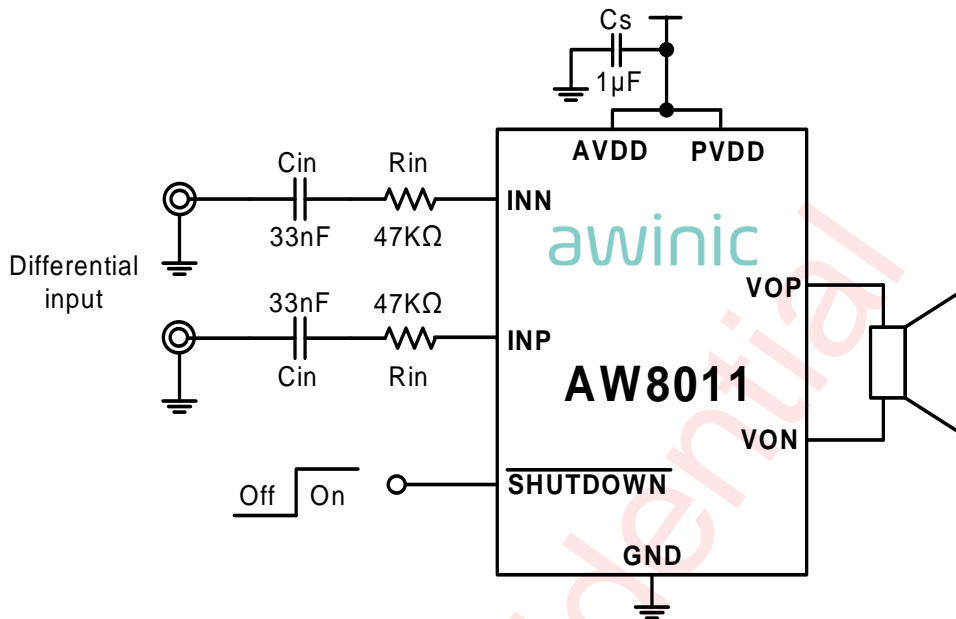


Figure 4 AW8011 Application Schematic With Differential Input

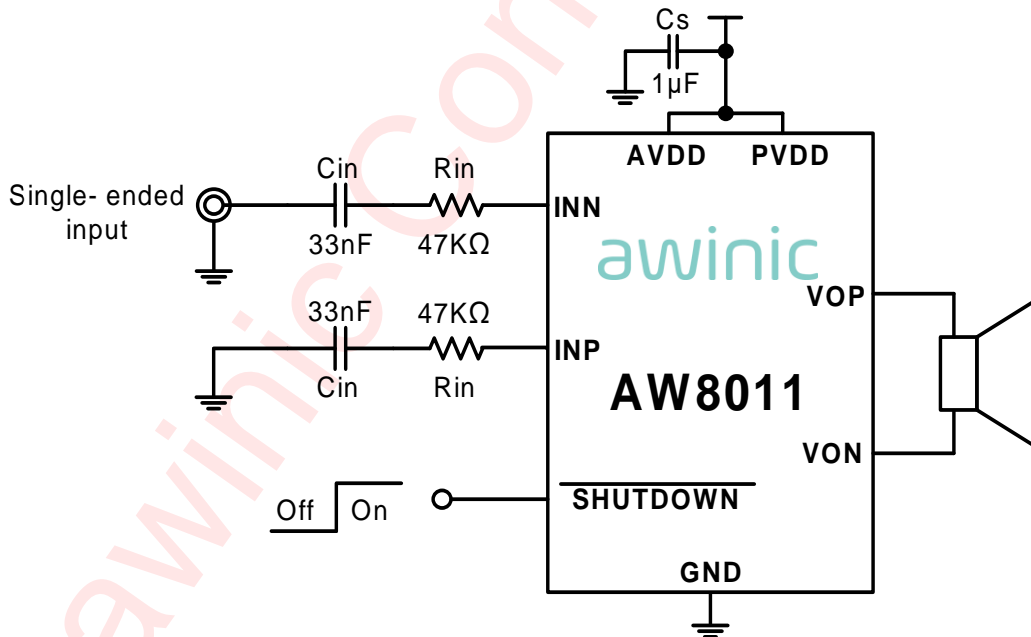


Figure 5 AW8011 Application Schematic With Single-Ended Input

## Ordering Information

Part Number	Temperature	Package	Marking	Moisture Sensitivity Level	Environmental Information	Delivery Form
AW8011CSR	-40°C~85°C	WLCSP 1.25mm×1.185mm× 0.582mm-9B	E1G	MSL1	ROHS+HF	4500 units/ Tape and Reel

## Absolute Maximum Ratings<sup>(NOTE1)</sup>

PARAMETERS	RANGE
Supply voltage range $V_{AVDD}/V_{PVDD}$	-0.3V to 6V
Input voltage range	-0.3V to $V_{AVDD}+0.3V$
Junction-to-ambient thermal resistance $\theta_{JA}$	90°C/W
Operating free-air temperature range	-40°C to 85°C
Maximum operating junction temperature $T_{JMAX}$	150°C
Storage temperature $T_{STG}$	-65°C to 150°C
Lead temperature (soldering 10 seconds)	260°C
ESD(Including CDM HBM MM) <sup>(NOTE 2)</sup>	
HBM (human body model)	±2kV
CDM (charged-device model)	±1.5kV
Latch-Up	
Test condition: JEDEC78E	+IT: 200mA -IT: -200mA

**NOTE1:** Conditions out of those ranges listed in "absolute maximum ratings" may cause permanent damages to the device. In spite of the limits above, functional operation conditions of the device should within the ranges listed in "recommended operating conditions". Exposure to absolute-maximum-rated conditions for prolonged periods may affect device reliability.

**NOTE2:** The human body model is a 100pF capacitor discharged through a 1.5kΩ resistor into each pin. Test method: ESDA/JEDEC JS-001-2017

Test method of the charged-device model: ESDA/JEDEC JS-002-2018

## Electrical Characteristics

Test Condition:  $V_{DD}=3.6V$ ,  $T_A=25^{\circ}C$ ,  $R_L=8\Omega+33\mu H$ ,  $C_{in}=33nF$ ,  $f=1kHz$  (Unless otherwise specified)

Parameter		Conditions	Min	Typ	Max	Units
<b>Electrical Characteristics</b>						
$V_{AVDD}, V_{PVDD}$	Power voltage		2.5		5.5	V
$V_{IH}$	High-level input voltage		1.3		VDD	V
$V_{IL}$	Low-level input voltage		0		0.35	V
$V_{OS}$	Output offset voltage	$V_{IN}=0V$	-25		25	mV
$I_Q$	Quiescent current	$V_{DD}=3.6V$		2.8		mA
$I_{SD}$	Shutdown current	$V_{DD}=3.6V$ , $\overline{SHUTDOWN}=0V$		0.1		$\mu A$
PSRR	Power supply rejection ratio	217Hz		75		dB
CMRR	Common mode rejection ratio			70		dB
$f_{SW}$	Switching frequency	$V_{DD}=2.5V$ to $5.5V$		800		kHz
$A_V$	Gain			$\frac{330k\Omega}{R_{in}}$		V/V
<b>Operating Characteristics</b>						
$P_O$	Output power (NCNOFF mode)	THD+N=10%, $R_L=4\Omega+33\mu H$ , $V_{DD}=5V$		2.85		W
		THD+N=1%, $R_L=4\Omega+33\mu H$ , $V_{DD}=5V$		2.31		W
		THD+N=10%, $R_L=8\Omega+33\mu H$ , $V_{DD}=5V$		1.66		W
		THD+N=1%, $R_L=8\Omega+33\mu H$ , $V_{DD}=5V$		1.35		W
		THD+N=10%, $R_L=4\Omega+33\mu H$ , $V_{DD}=4.2V$		1.97		W
		THD+N=1%, $R_L=4\Omega+33\mu H$ , $V_{DD}=4.2V$		1.60		W
		THD+N=10%, $R_L=8\Omega+33\mu H$ , $V_{DD}=4.2V$		1.16		W
		THD+N=1%, $R_L=8\Omega+33\mu H$ , $V_{DD}=4.2V$		0.94		W
		THD+N=10%, $R_L=4\Omega+33\mu H$ , $V_{DD}=3.6V$		1.41		W
		THD+N=1%, $R_L=4\Omega+33\mu H$ , $V_{DD}=3.6V$		1.14		W
		THD+N=10%, $R_L=8\Omega+33\mu H$ , $V_{DD}=3.6V$		0.84		W
		THD+N=1%, $R_L=8\Omega+33\mu H$ , $V_{DD}=3.6V$		0.68		W
$E_N$	Output noise	Gain=6V/V, 20Hz to 20kHz, input ac grounded, A-weighting		46		$\mu V$
THD+N	Total harmonic distortion plus noise	$V_{DD}=5V$ , $P_O=0.6W$ , $R_L=8\Omega+33\mu H$		0.008		%
		$V_{DD}=4.2V$ , $P_O=0.4W$ , $R_L=8\Omega+33\mu H$		0.008		%
		$V_{DD}=3.6V$ , $P_O=0.3W$ , $R_L=8\Omega+33\mu H$		0.008		%
$\eta$	Efficiency	$V_{DD}=5V$ , $P_O=1W$ , $R_L=8\Omega+33\mu H$		85		%
$t_{ST}$	Start-up time			40		ms
$t_{OFF}$	Turn-off time			4		$\mu s$

## MEASUREMENT SETUP

AW8011 features switching digital output, as shown in Figure 6. Need to connect a low pass filter to VOP/VON output respectively to filter out switch modulation frequency, then measure the differential output of filter to obtain analog output signal.

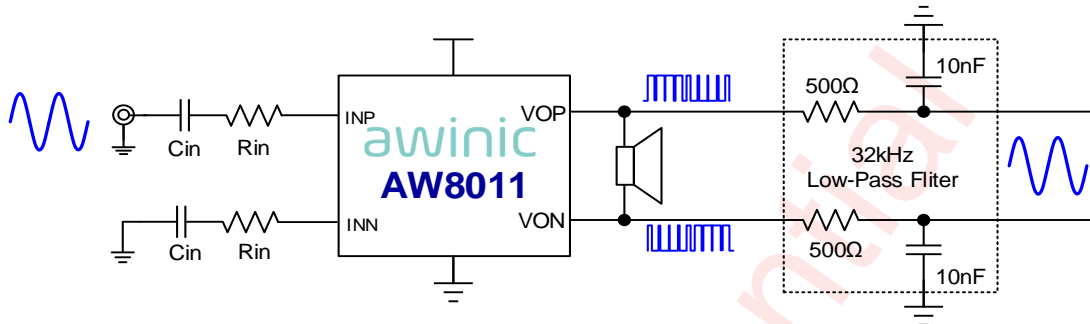


Figure 6 AW8011 test setup

Low pass filter uses resistance and capacitor values listed in Table 1.

Table 1 AW8011 recommended values for low pass filter

R <sub>filter</sub>	C <sub>filter</sub>	Low-pass cutoff frequency
500Ω	10nF	32kHz
1kΩ	4.7nF	34kHz

### Output Power Calculation

According to the above test methods, the differential analog output signal is obtained at the output of the low pass filter. The valid values Vo<sub>rms</sub> of the differential signal as shown below:

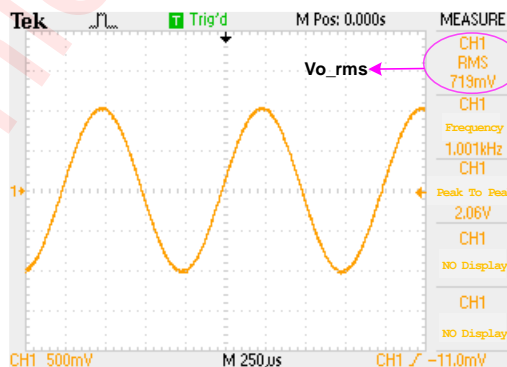
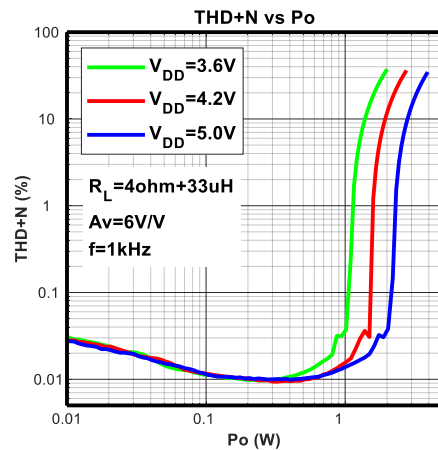
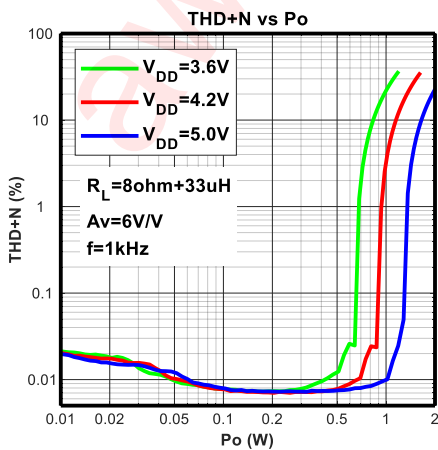
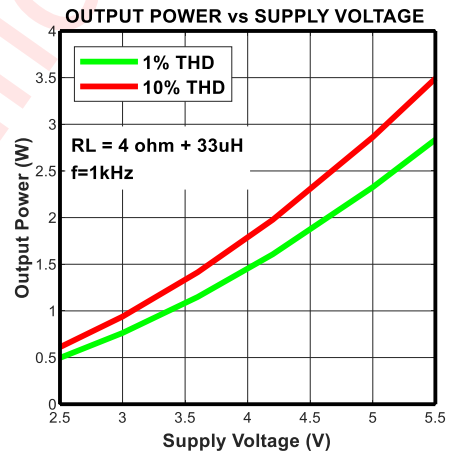
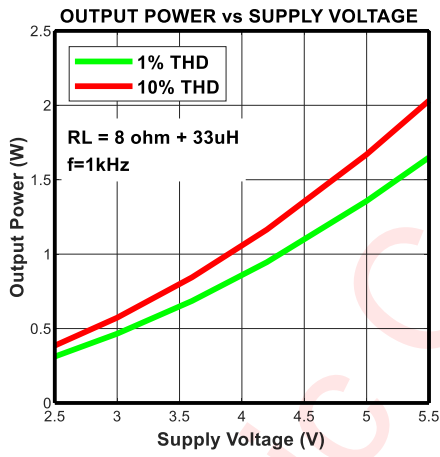
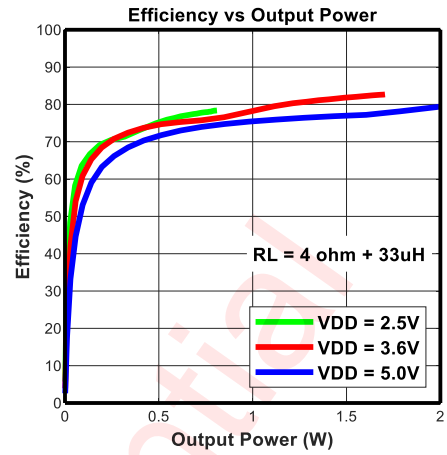
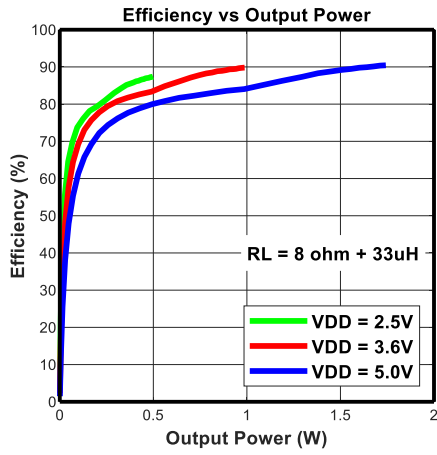


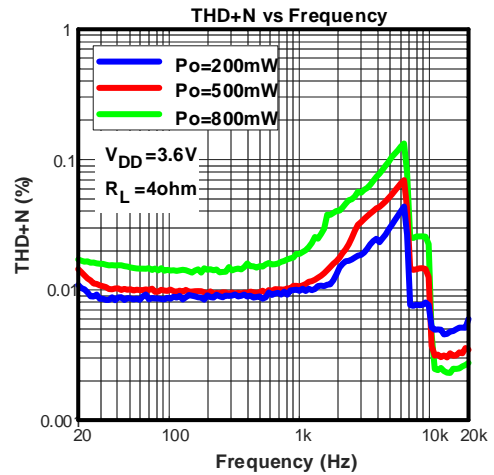
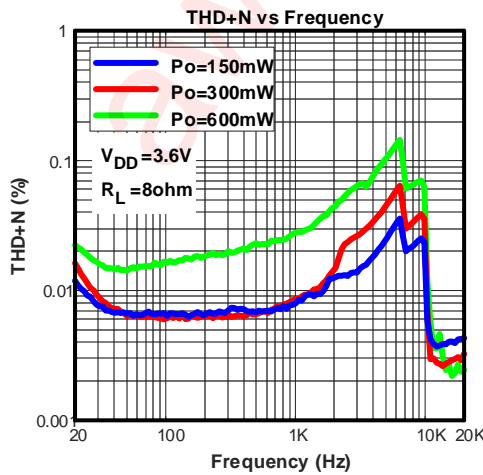
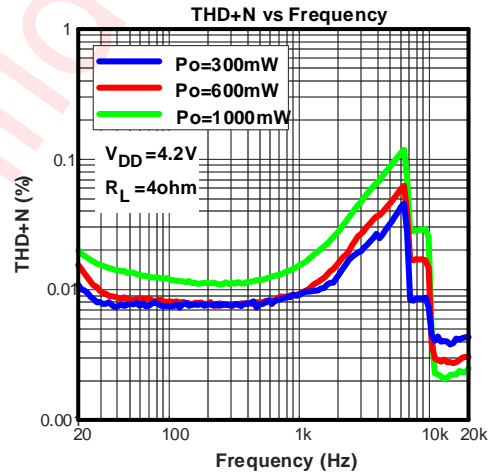
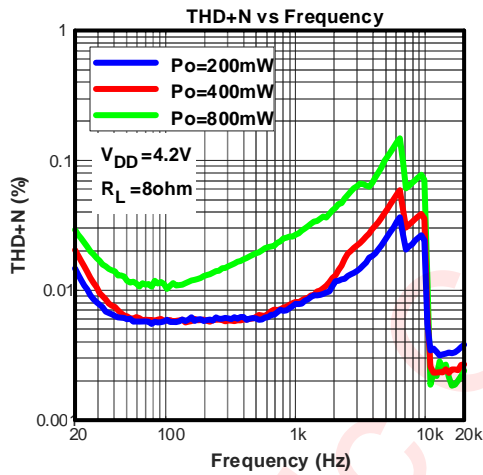
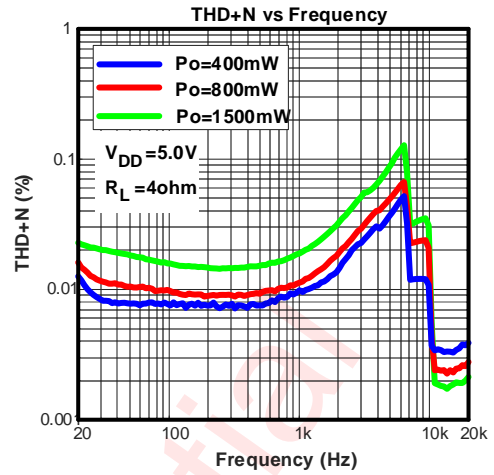
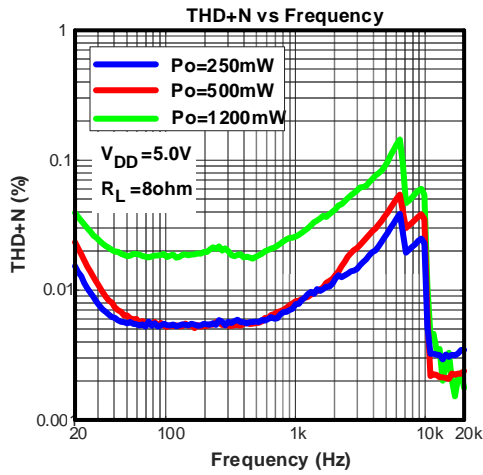
Figure 7 Valid value of AW8011 output signal

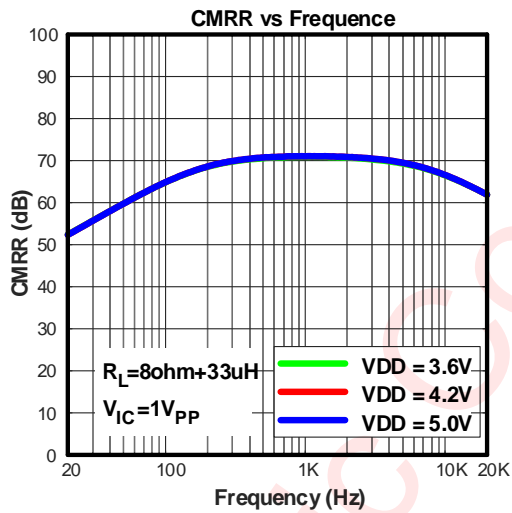
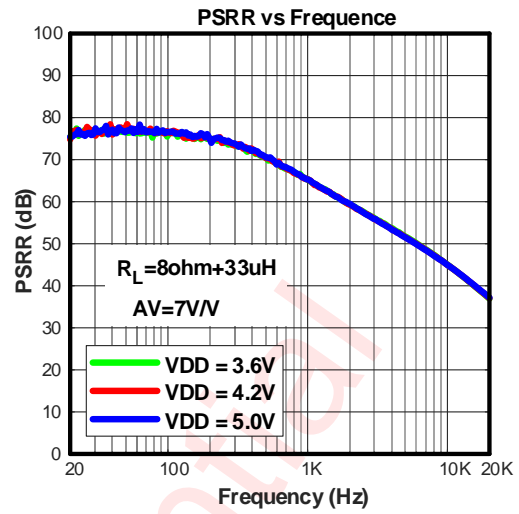
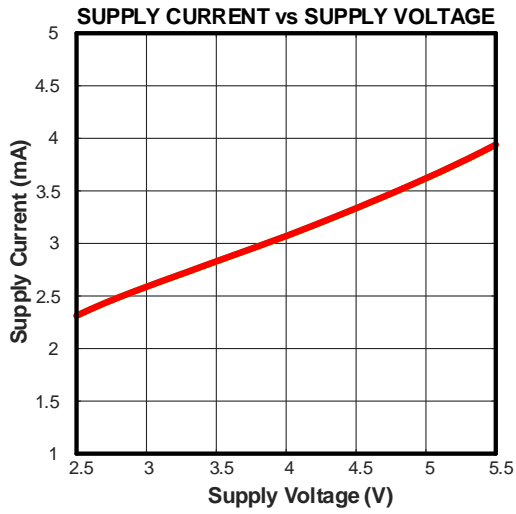
The power calculation of Speaker is as follows:

$$P_L = \frac{(V_{o\_rms})^2}{R_L} \quad (R_L: \text{load impedance of the speaker})$$

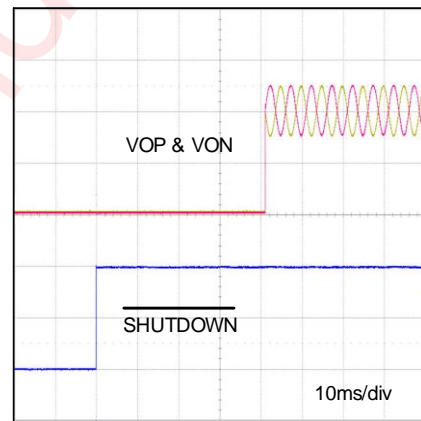
### Typical Characteristics



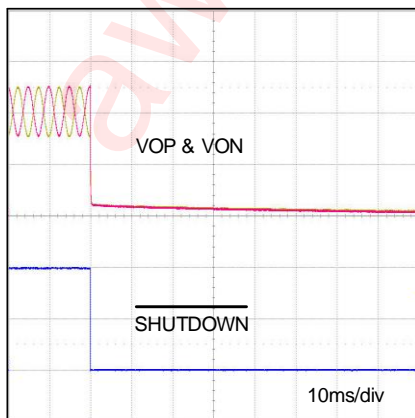




Start up time



Shutdown time



## Detailed Functional Description

The AW8011 is a ultra-low-EMI,RNS, mono, filter-free, Class-D audio amplifier. Unique RNS, which effectively reduces RF energy, attenuate the RF TDD-noise, an acceptable audible level to the customer.

The AW8011 features the EEE (Enhanced Emission Elimination) function which greatly reduces EMI over the full bandwidth. The AW8011 achieves better than 20dB margin under FCC limits with 24 inch of cable.

The filter-free PWM architecture and internal gain setting reduces external components count, board area consumption, system cost and simplifies the design. The over-current and over-temperature protection is prepared inside of the device, which prevent the device from damage during fault conditions. When the fault condition is removed, the AW8011 reactivate itself again.

### FILTER-FREE MODULATION SCHEME

The AW8011 features a filter-free PWM architecture that reduces the LC filter of the traditional Class-D amplifier, increasing efficiency, reducing board area consumption and system cost.

### POP-CLICK SUPPRESSION

The AW8011 features unique timing control circuit, that comprehensively suppresses pop-click noise, eliminates audible transients on shutdown, wakeup, and power-up/down

### EEE TECHNOLOGY

The AW8011 features a unique Enhanced Emission Elimination (EEE) technology, that controls fast transition on the output, greatly reduces EMI over the full bandwidth. The AW8011 achieves better than 20dB margin under FCC limits with 24 inch of cable.

### EFFICIENCY

Efficiency of a Class D amplifier is attributed to the switching operation of the output stage transistors. In a Class D amplifier, the output transistors act as current steering switches and consume negligible additional power. Any power loss associated with the Class D output stage is mostly due to the  $I^2R$  loss of the MOSFET on-resistance and supply current. The AW8011 features efficiency of 90%.

### PROTECTION FUNCTION

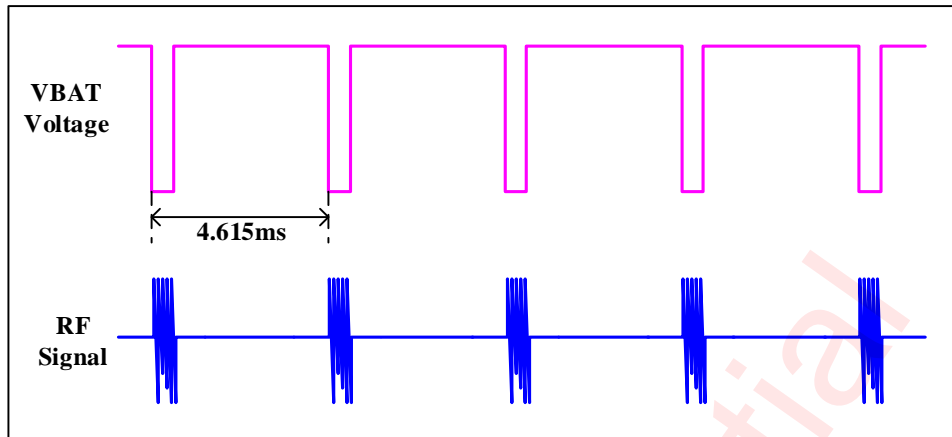
When a short-circuit occurs between VOP/VON pin and VDD/GND or VOP and VON, the over-current circuit shutdown the device, preventing the device from being damaged. When the condition is removed, the AW8011 reactivate itself. When the junction temperature is high, the over-temperature circuit shutdown the device. The circuit switches back to normal operation when the temperature decreases to safe level.

### RNS(RF TDD NOISE SUPPRESSION)

#### TDD Noise Causes

GSM cell phones use TDMA (Time Division Multiple Access) slot sharing technology. The time is divided into periodic frames in TDMA, and each frame is subdivided into a plurality of time slots. In order to transmit signals to the base station, the signals sent from the base stations to the plurality of mobile terminals are arranged in a predetermined time slot in the transmission. In this case, each TDMA frame contains 8 time slots, the entire frame is about 4.615ms long, and each slot time is 0.577ms.

With GSM handset, the RF power amplifier will transmit once every 4.615ms (217Hz), and the signal will produce intermittent Burst current and strong electromagnetic radiation. Intermittent Burst current will form a power fluctuation of 217 Hz; High frequency (900MHz and 1800MHz) RF signals form a 217Hz RF envelope signal. 217Hz power fluctuations will be conducted through the conduction to the audio signal path, 217Hz RF envelope signal will be coupled through the radiation into the audio signal path, if the protection is not good, it will produce an audible TDD Noise, which includes the 217Hz noise And a harmonic noise signal of 217 Hz.



**Figure 8 Schematic Diagram of Power Supply Voltage and RF Signal during GSM RF Operation**

RNS fully inhibit the conduction and radiation interference by the AWINIC unique circuit architecture. Effectively improve the ability to suppress TDD Noise.

### Conduction noise suppression

When the RF power amplifier is operating, it will draw the current from the battery by 217Hz frequency, Power supply will be introduced to 217Hz power ripple since the battery has a certain internal resistance, it will be coupled to the speaker through the audio power amplifier. The ability to suppress power fluctuations depends on the PSRR of the audio power amplifier.

$$PSRR = 20 \log\left(\frac{v_{dd\_ac}}{v_{out\_ac}}\right)$$

Due to the input and output of the fully differential amplifier is perfectly symmetrical, theoretically, the effect of the power supply fluctuation on the two outputs is exactly the same, and the differential output is completely unaffected by the power supply fluctuation. In practice, due to process bias and other factors, the amplifier will have a certain mismatch, PSRR is generally better than 60dB, it shows the output relative to the power fluctuations can be reduced by 1000 times, such as 500mVp power fluctuations, the differential output of 0.5 mV, which basically can meet the application requirements.

But in practical applications, the power amplifier may encounter conduction of TDD Noise problem even if its PSRR is 60dB or 80dB, why is this? Because we also need to consider the impact of peripheral power mismatches of audio power amplifiers.

For conventional audio power amplifiers, when the input resistor  $R_{in}$  and the input capacitor  $C_{in}$  mismatch, will greatly affect the audio power amplifier PSRR indicators, in the case of 24 times gain, PSRR will be weakened to 46dB or so if the input resistance and Capacitor with 1% mismatch. PSRR will be weakened to 28dB or so if the input resistance and input capacitance mismatch with 10% mismatch, when the power fluctuations, it is easy to produce audible TDD Noise.

In order to enhance the audio power amplifier PSRR in the input resistance and input capacitance mismatch case, AW8011 features a unique conduction noise suppression circuit, making the power amplifier to maintain a high PSRR value even in the input resistance, the input capacitance deviation of 10% or more, this greatly inhibits the generation of conducted noise.

## Radiation noise suppression

Input traces, output traces, horn loops, and even power and ground loops are likely to be subject to RF radiation interference in the audio signal module, longer input traces and output traces similar to the antenna, especially vulnerable RF radiation effects.

The reasonable PCB layout can reduce the influence of RF radiation in the design, such as shorten the line length of input and output as much as possible; audio devices should be shielded and far away from the RF antenna, maintain the integrity of the device to audio signal pathway; to increase the small bypass capacitor RF signals in the sensitive nodes. However, in practical applications, PCB layout is difficult to fully consider the influence of RF radiation on the audio signal path, and some RF energy will still be coupled to the audio signal path to form audible TDD Noise. Therefore, AW8011 features a unique RF radiation suppression circuit, a shielding layer inside the chip, effectively prevent high frequency energy into RF chip, to ensure that the drive signal of the amplifier provided to the speaker will not be affected by the antenna RF radiation, thus avoiding the antenna RF Radiation caused by TDD Noise.

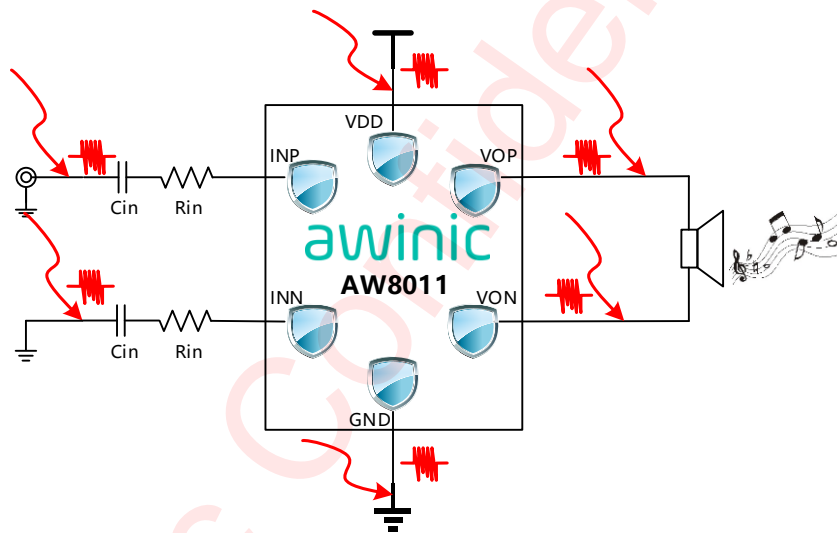


Figure 9 RF Energy Coupling Diagram

## Application Information

### SUPPLY DECOUPLING CAPACITOR

The AW8011 is a high-performance class-D audio amplifier that requires adequate power supply decoupling to ensure the efficiency is high and total harmonic distortion (THD) is low. For higher frequency transients, a good low equivalent-series-resistance (ESR) ceramic capacitor, typically 1 $\mu$ F, placed as close as possible to the device VDD pin works best. For filtering lower-frequency noise signals, a 10  $\mu$ F or greater capacitor placed near the audio power amplifier would also help.

### INPUT RESISTORS

The input resistors set the gain of the amplifier according to equation as follow.

$$Gain = \frac{2 \times 165 k\Omega}{R_{in}} \left( \frac{V}{V} \right)$$

The resistors matching is very important. CMRR, PSRR and THD diminish if resistor mismatch occurs. Therefore, it is recommended use 1% tolerance resistors or better to keep the performance optimized. Place the input resistors very close to the AW8011 to limit noise injection on the high-impedance nodes.

### INPUT CAPACITOR

The input coupling capacitor blocks the DC voltage at the amplifier input terminal. The input capacitors and input resistors form a high-pass filter with the corner frequency,  $f_c$ .

$$f_c = \frac{1}{2\pi R_{in} C_{in}}$$

Setting the high-pass filter point high can block the 217Hz GSM noise coupled to inputs. Better matching of the input capacitors improves performance of the circuit and also help to suppress pop-click noise.

### FERRITE CHIP BEAD AND CAPACITOR

The AW8011 passed FCC and CE radiated emissions with no ferrite chip beads and capacitors with speaker trace wires 24 inch. Use ferrite chip beads and capacitors if device near the EMI sensitive circuits and/or there are long leads from amplifier to speaker, placed as close as possible to the output pin.

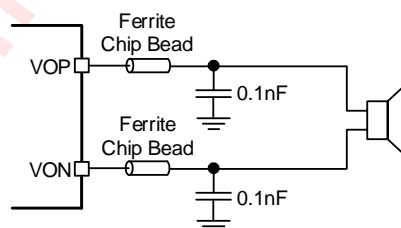
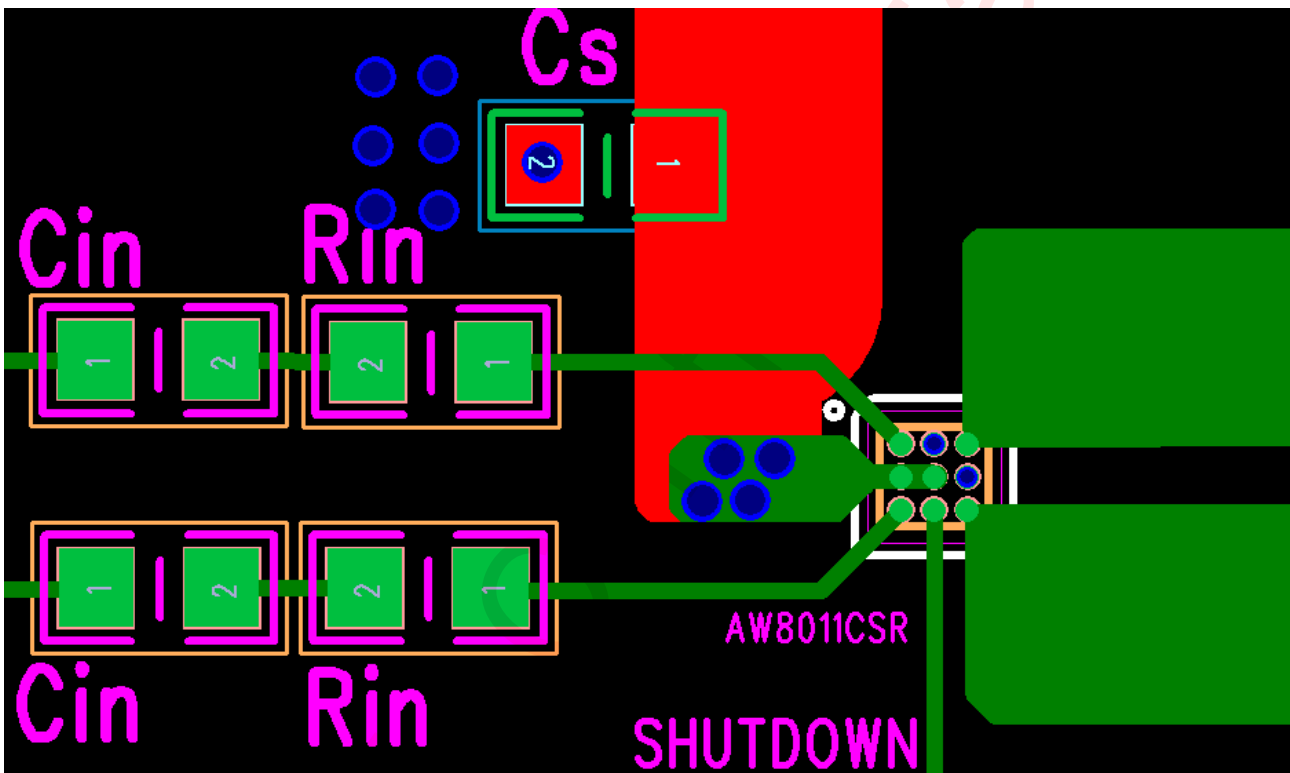


Figure 10 Ferrite Chip Bead and capacitor

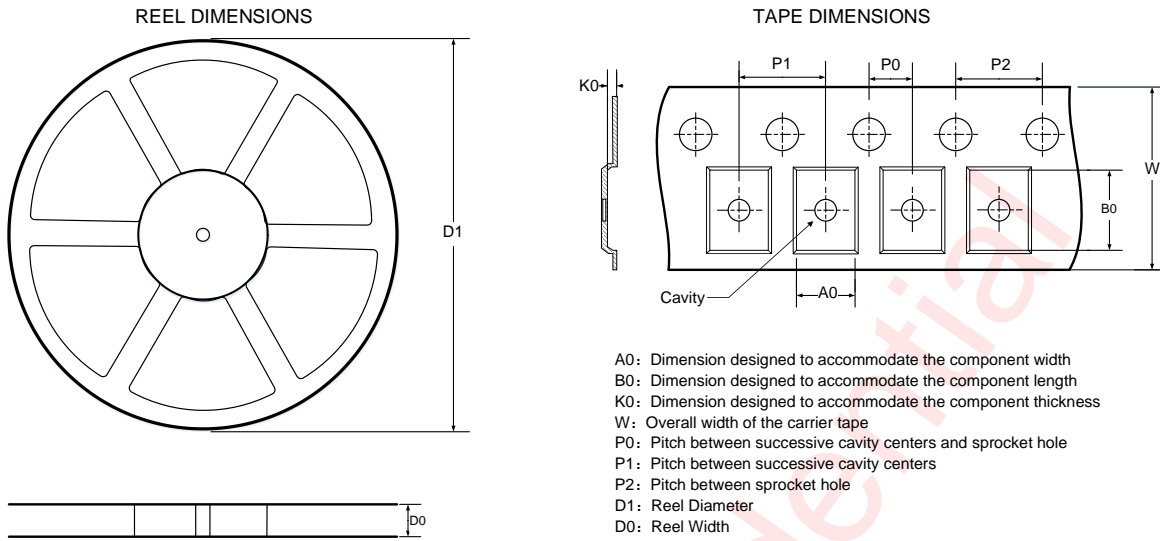
## PCB Layout Consideration

In order to obtain excellent performance of AW8011, PCB layout must be carefully considered. The design consideration should follow the following principles:

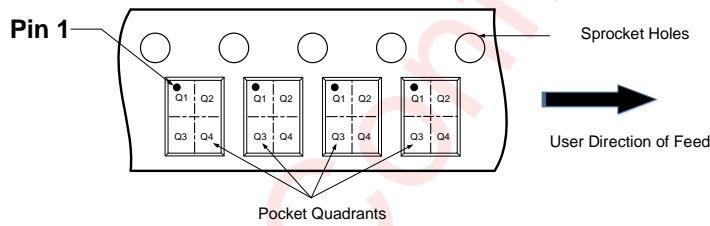
1. Try to provide a separate short and thick power line to AW8011, the copper width is recommended to be larger than 1.2mm. The decoupling capacitors should be placed as close as possible to power supply pin.
2. The input capacitors and resistors should be close to AW8011 INN and INP input pin, the input line should be parallel to suppress noise coupling.



## Tape And Reel Information



QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



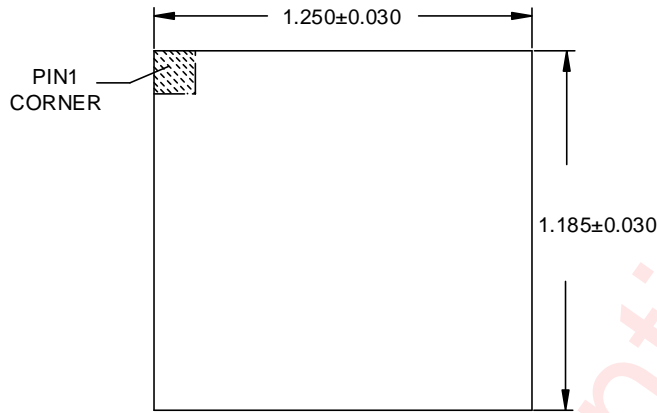
Note: The above picture is for reference only. Please refer to the value in the table below for the actual size

DIMENSIONS AND PIN1 ORIENTATION

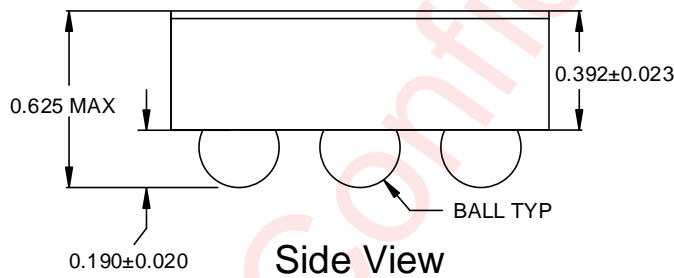
D1 (mm)	D0 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P0 (mm)	P1 (mm)	P2 (mm)	W (mm)	Pin1 Quadrant
178	8.4	1.35	1.35	0.76	2	4	4	8	Q1

All dimensions are nominal

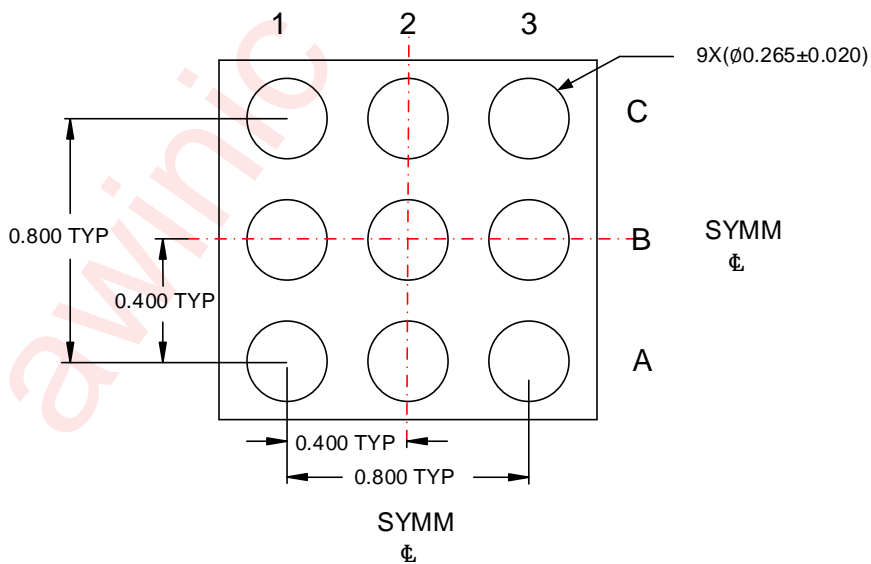
Package Description



Top View



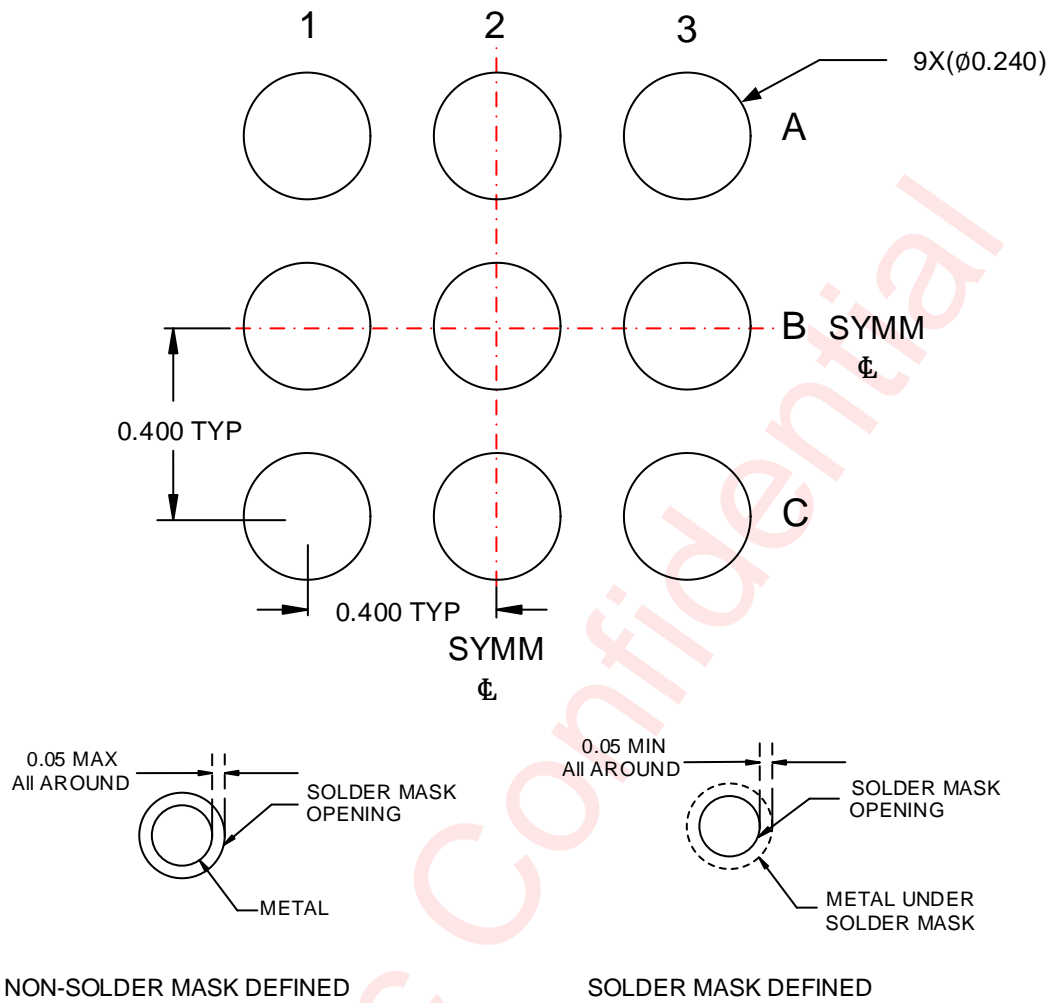
Side View



Bottom View

Unit: mm

Land Pattern Data



Unit: mm

## Revision History

Version	Date	Change Record
V1.0	Aug. 2022	Officially released
V1.1	Oct. 2022	Upgrade parameters
V1.2	Dec. 2022	Upgrade parameters
V1.3	Mar. 2023	Upgrade $V_{PVDD}/V_{AVDD}$ description

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