

SK6252B 17V 2A 500KHz Force-CCM Sync Step-Down Regulator

GENERAL DESCRIPTION

The SK6252B is a high frequency, synchronous, rectified, step-down, switch-mode converter with internal power MOSFETs. It offers a very compact solution to provide 2A continuous output current over wide input supply range with excellent load and line regulation.

eCOT control operation provides very fast transient response and easy loop design as well as very tight output regulation.

The SK6252B is available in SOT23-6 package.

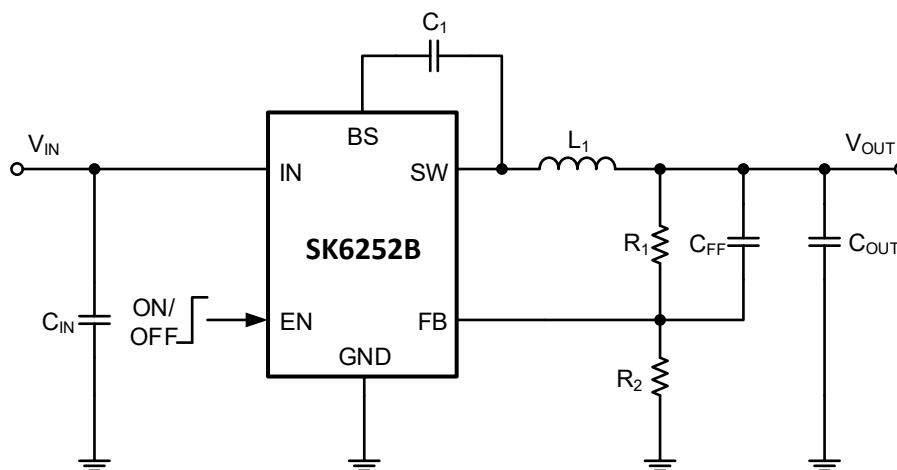
APPLICATIONS

- Set-top Boxes
- LCD TVs
- Home Networking Devices
- Surveillance
- General Purposes

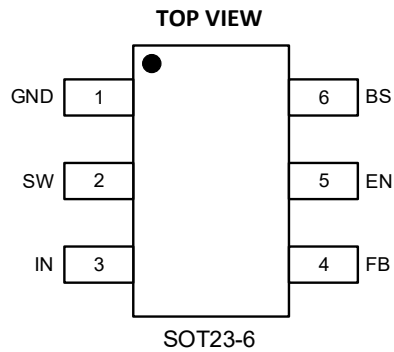
FEATURES

- Wide Input Voltage Range: 4.5V to 17V
- Continuous Output Current: 2A
- Switching Frequency: 500KHz
- Feedback Voltage: 0.765V
- eCOT Mode Control with Fast Transient Response
- Built-in Over Current Limit
- Built-in Over Voltage Protection
- Continuous Conduction Mode (CCM)
- Internal Soft-Start
- No Schottky Diode Required
- Short Protection with Hiccup-Mode
- Integrated Internal Compensation
- Thermal Shutdown
- -40°C to +85°C Temperature Range

TYPICAL APPLICATION CIRCUIT



PIN CONFIGURATION



PIN DESCRIPTIONS

Pin	Name	Function
1	GND	Ground Pin
2	SW	Switching Pin
3	IN	Power Supply Pin
4	FB	Feedback input. Connect FB to the center of the external resistor divider.
5	EN	Drive this pin to a logic-high to enable the IC. Drive to a logic-low to disable the IC and enter micro-power shutdown mode.
6	BS	Supply input for the high-side MOSFET gate drive circuit. Connect 0.1 μ F (typical) capacitor between BS and SW pins.

ORDERING INFORMATION

Part Number	Package	VFB	Quantity/ Reel
SK6252B	SOT23-6	0.765V	3000

SK6252B devices are Pb-free and RoHS compliant.

ABSOLUTE MAXIMUM RATINGS ⁽¹⁾⁽²⁾

Item	Min	Max	Unit
V _{IN} voltage	-0.3	18	V
EN voltage	-0.3	18	V
SW voltage	-3	19	V
SW voltage (<10 ns transient)	-5	19	V
BS voltage (to SW)	-0.3	6.5	V
FB voltage	-0.3	6	V
Power dissipation	Internally Limited		
Operating junction temperature, T _J	-40	150	°C
Storage temperature, T _{stg}	-55	150	°C
Lead Temperature (Soldering, 10sec.)		260	°C

Note (1): Exceeding these ratings may damage the device.

Note (2): The device is not guaranteed to function outside of its operating conditions.

ESD Ratings

Item	Description	Value	Unit
V _(ESD-HBM)	Human Body Model (HBM) ANSI/ ESDA/JEDEC JS-001-2014 Classification, Class: 2	±2000	V
V _(ESD-CDM)	Charged Device Mode (CDM) ANSI/ESDA/JEDEC JS-002-2014 Classification, Class: C0b	±200	V
I _{LATCH-UP}	JEDEC STANDARD NO.78E APRIL 2016 Temperature Classification, Class: I	±150	mA

THERMAL INFORMATION

Item	Description	Value	Unit
R _{θJA}	Junction-to-ambient thermal resistance ⁽¹⁾⁽²⁾	105	°C/W
R _{θJC(top)}	Junction-to-case (top) thermal resistance	55	°C/W
R _{θJB}	Junction-to-board thermal resistance	17.5	°C/W
ψ _{JT}	Junction-to-top characterization parameter	3.5	°C/W
ψ _{JB}	Junction-to-board characterization parameter	17.5	°C/W

Note (1): The package thermal impedance is calculated in accordance to JESD 51-7.

Note (2): Thermal Resistances were simulated on a 4-layer, JEDEC board.

RECOMMENDED OPERATING CONDITIONS

Item	Min	Max	Unit
Operating junction temperature ⁽¹⁾	-40	125	°C
Operating temperature range	-40	85	°C
Input voltage V_{IN}	4.5	17	V
Input voltage EN	-0.1	17	V
BST voltage	-0.1	21	V
FB voltage	-0.1	6	V
Output current	0	2	A

Note (1): All limits specified at room temperature ($T_A = 25^\circ\text{C}$) unless otherwise specified. All room temperature limits are 100% production tested. All limits at temperature extremes are ensured through correlation using standard Statistical Quality Control (SQC) methods. All limits are used to calculate Average Outgoing Quality Level (AOQL).

ELECTRICAL CHARACTERISTICS ^{(1) (2)}

$V_{IN}=12\text{V}$, $T_A=25^\circ\text{C}$, unless otherwise specified.

Parameter	Test Conditions	Min	Typ.	Max	Unit
Input Voltage Range		4.5		17	V
Output Voltage Range		0.765		7	V
Supply Current (Quiescent)	$V_{EN}=3.0\text{V}$		0.6	0.8	mA
Supply Current (Shutdown)	$V_{EN}=0$ or $EN = \text{GND}$			4	uA
Feedback Voltage		0.746	0.765	0.784	V
High-Side Switch On-Resistance	$I_{SW}=100\text{mA}$		110		mΩ
Low-Side Switch On-Resistance	$I_{SW}=-100\text{mA}$		70		mΩ
Valley Switch Current Limit			2		A
Output UVP threshold	Hiccup detect ($H > L$)		60		%
Hiccup wait time			1.8		ms
Hiccup time before restart			32		ms
Over Voltage Protection Threshold			18		V
Switching Frequency			500		KHz
Maximum Duty Cycle	$V_{FB}=90\%$		90		%
Minimum Off-Time			200		nS
EN Rising Threshold		1.4			V
EN Falling Threshold				0.8	V
Under-Voltage Lockout Threshold	Wake up V_{IN} Voltage		4.3	4.5	V
	Shutdown V_{IN} Voltage	3.6	3.8		V
	Hysteresis V_{IN} voltage		500		mV
Soft Start			1.5		mS
Thermal Shutdown			160		°C
Thermal Hysteresis			30		°C

Note (1): MOSFET on-resistance specifications are guaranteed by correlation to wafer level measurements.

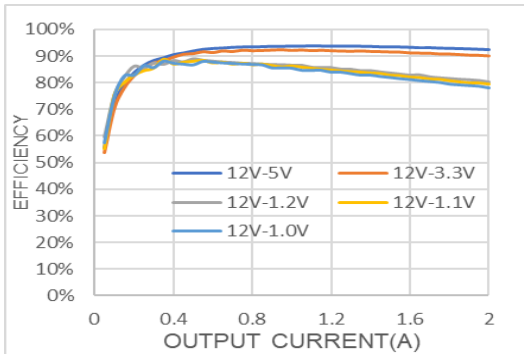
Note (2): Thermal shutdown specifications are guaranteed by correlation to the design and characteristics analysis.

TYPICAL PERFORMANCE CHARACTERISTICS

$V_{IN}=12V$, $V_{OUT}=3.3V$, $T_A=+25^{\circ}C$, unless otherwise noted. Performance waveforms are tested on the evaluation board.

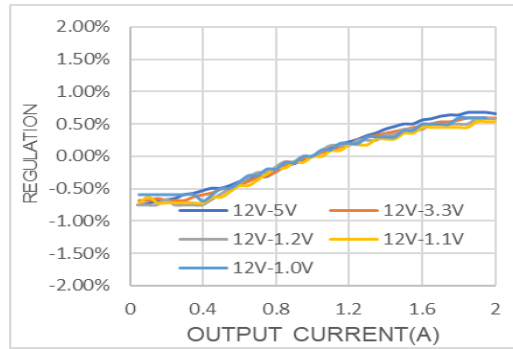
Efficiency vs Load Current

$V_{OUT}=5V, 3.3V, 1.2V, 1.1V, 1.0V$



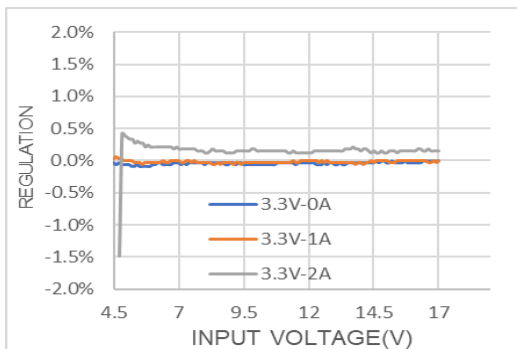
Load Regulation

$V_{OUT}=5V, 3.3V, 1.2V, 1.1V, 1.0V$



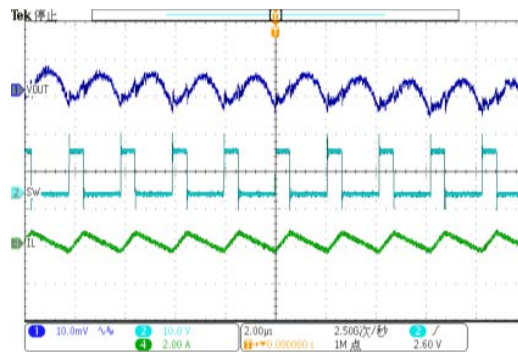
Line Regulation

$V_{OUT}=3.3V$



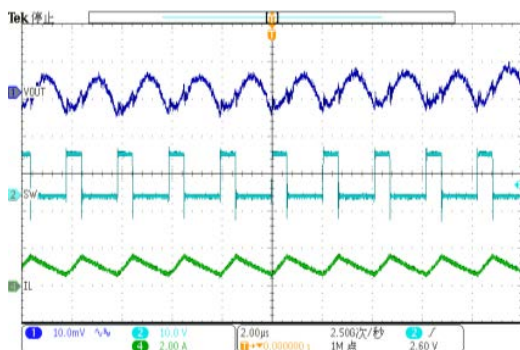
Output Ripple Voltage

$V_{IN}=12V$, $V_{OUT}=3.3V$, $I_{OUT}=0A$



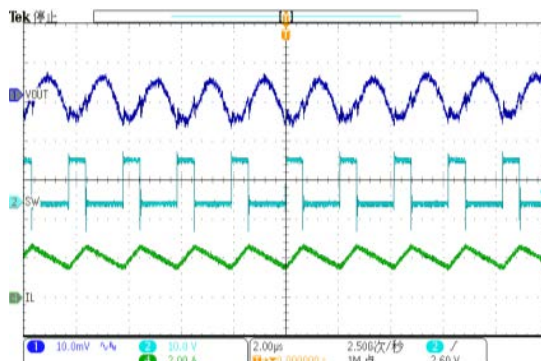
Output Ripple Voltage

$V_{IN}=12V$, $V_{OUT}=3.3V$, $I_{OUT}=1A$

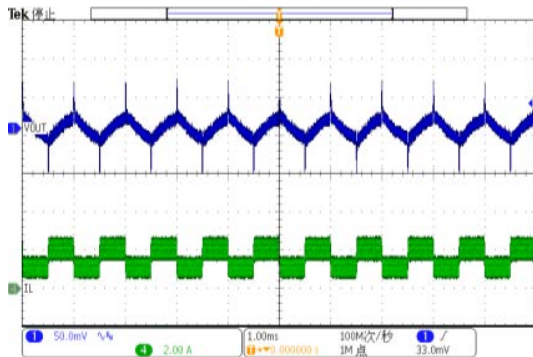


Output Ripple Voltage

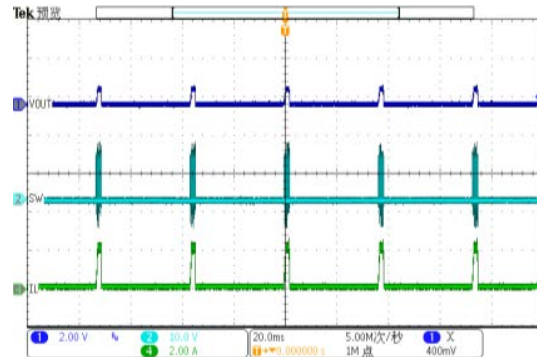
$V_{IN}=12V$, $V_{OUT}=3.3V$, $I_{OUT}=2A$



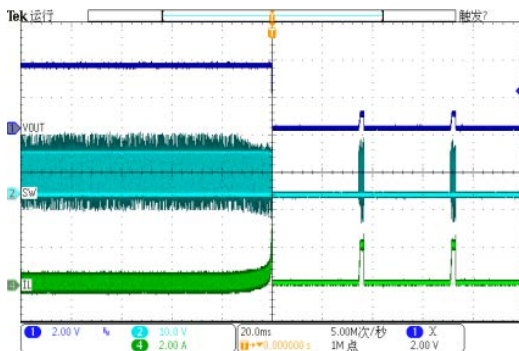
Loop Response

 $V_{IN}=12V$, $V_{OUT}=3.3V$, $I_{OUT}=1A-2A$


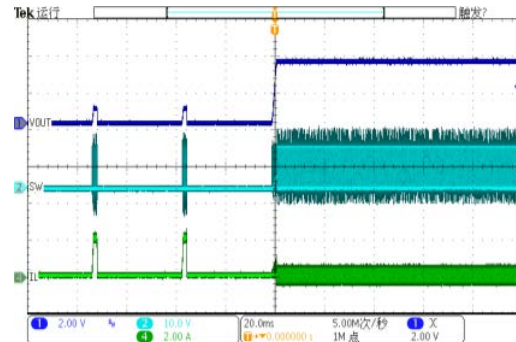
Output Short

 $V_{IN}=12V$, $V_{OUT}=3.3V$


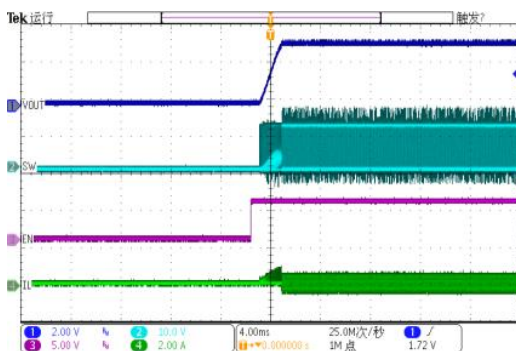
Short Circuit Entry

 $V_{IN}=12V$, $V_{OUT}=3.3V$


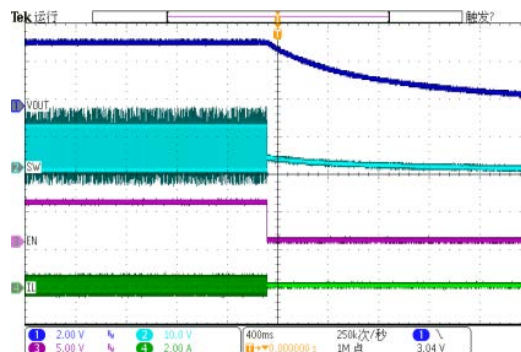
Short Circuit Recovery

 $V_{IN}=12V$, $V_{OUT}=3.3V$


Enable Startup at No Load

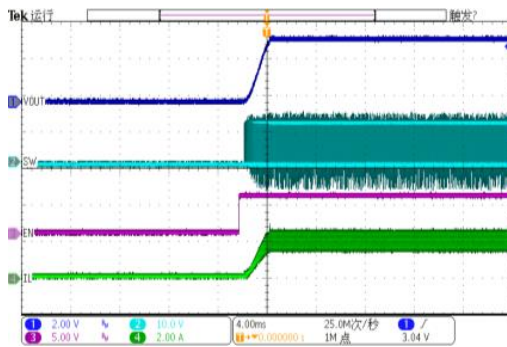
 $V_{IN}=12V$, $V_{OUT}=3.3V$, $I_{OUT}=0A$


Enable Shutdown at No Load

 $V_{IN}=12V$, $V_{OUT}=3.3V$, $I_{OUT}=0A$


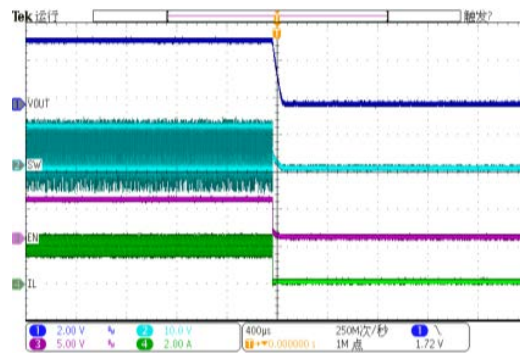
Enable Startup at Full Load

$V_{IN}=12V$, $V_{OUT}=3.3V$, $I_{OUT}=2A$



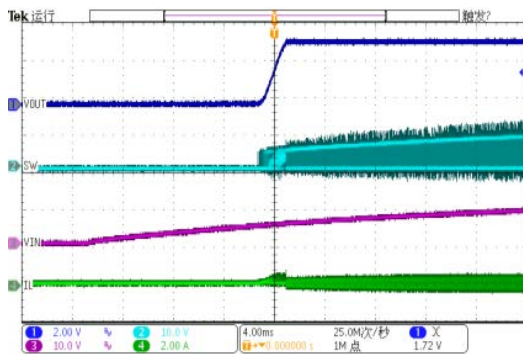
Enable Shutdown at Full Load

$V_{IN}=12V$, $V_{OUT}=3.3V$, $I_{OUT}=2A$



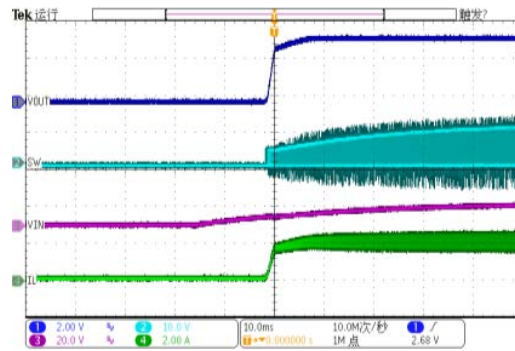
Power Up at No Load

$V_{IN}=12V$, $V_{OUT}=3.3V$, $I_{OUT}=0A$

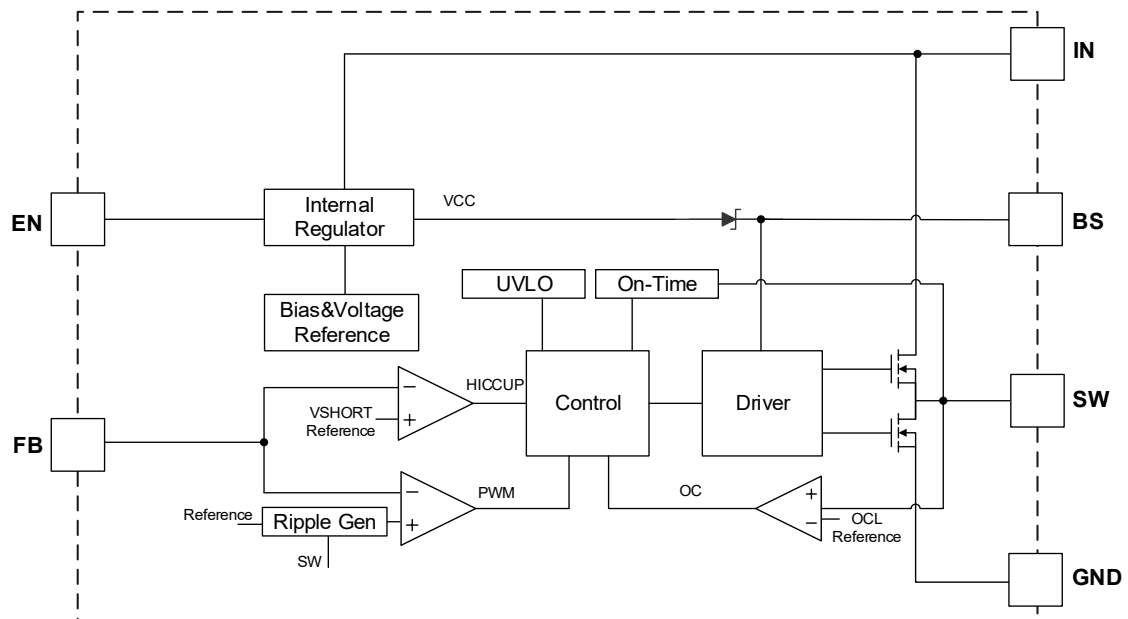


Power Up at Full Load

$V_{IN}=12V$, $V_{OUT}=3.3V$, $I_{OUT}=2A$



BLOCK DIAGRAM



FUNCTIONS DESCRIPTION

Internal Regulator

The SK6252B is an eCOT mode step down DC/DC converter which provides excellent transient response with no extra external compensation components. This device contains an internal, low resistance, high voltage power MOSFET, and operates at a high 500KHz frequency to ensure a compact, high efficiency design with excellent AC and DC performance.

Error Amplifier

The error amplifier compares the FB pin voltage with the internal reference (V_{FB}) and outputs a current proportional to the difference. This output current is then used to charge or discharge the internal compensation network, which is used to control the power MOSFET current. The optimized internal compensation network minimizes the external component counts and simplifies the control loop design.

Under-Voltage Lockout (UVLO)

Under-voltage lockout (UVLO) protects the chip from operating at insufficient supply voltage. UVLO protection monitors the internal regulator voltage. When the voltage is lower than UVLO threshold voltage, the device shuts off. When the voltage is higher than UVLO threshold voltage, the device is enabled again.

Thermal Shutdown

Thermal shutdown prevents the chip from operating at exceedingly high temperature. When the silicon die temperature exceeds 160°C, it shuts down the whole chip. When the temperature falls below its lower threshold (Typ. 130°C) the chip is enabled again.

Internal Soft-Start

The soft-start is implemented to prevent the converter output voltage from overshooting during startup. When the chip starts, the internal circuitry generates a soft-start voltage (SS) ramping up from 0V to 0.765V. When it is lower than the internal reference (REF), SS overrides REF so that the error amplifier uses SS as the reference. When SS is higher than REF, REF regains control. The SS time is internally set to 1.5ms.

Over Current Protection and Hiccup

The SK6252B employs a cycle-by-cycle over current limit; when the inductor current valley value exceeds the set current limit threshold, meanwhile, output voltage starts to drop until FB is below the Under-Voltage (UV) threshold, a UV event is triggered, the SK6252B enters hiccup mode to periodically restart. This protection mode is especially useful when the output is dead-short to ground. The average short circuit current is greatly reduced to alleviate the thermal issue and to protect the regulator. The SK6252B exits the hiccup mode once the over current condition is removed.

Startup and Shutdown

If both V_{IN} and EN are higher than the appropriate thresholds, the chip starts. The reference block starts first, generates stable reference voltage and currents, and then the internal regulator is enabled. The regulator provides stable supply for the remaining circuitries. Three events can shut down the chip: EN low, V_{IN} low and thermal shutdown. In the shutdown procedure, the signaling path is first blocked to avoid any fault triggering. The comp voltage and the internal supply rail are then pulled down. The floating driver is not subject to this shutdown command.

APPLICATION INFORMATION

Setting the Output Voltage

SK6252B requires an input capacitor, an output capacitor and an inductor. These components are CRITICAL to the performance of the device. SK6252B is internally compensated and does not require any external components to achieve a stable operation. The output voltage can be programmed by resistor divider.

$$V_{OUT} = V_{FB} \times \frac{R1 + R2}{R2}$$

V _{OUT} (V)	R1(KΩ)	R2(KΩ)	L1(μH)	C1(nF)	C _{IN} (μF)	C _{OUT} (μF)	C _{FF} (pF) Opt.
1.0	3.07	10	2.2	100	22	22×2	C_{FF} Chapter
1.05	3.73	10	2.2	100	22	22×2	C_{FF} Chapter
1.2	5.69	10	2.2	100	22	22×2	C_{FF} Chapter
1.5	9.61	10	2.2	100	22	22×2	C_{FF} Chapter
1.8	13.53	10	3.3	100	22	22×2	C_{FF} Chapter
2.5	22.68	10	4.7	100	22	22×2	C_{FF} Chapter
3.3	33.14	10	4.7	100	22	22×2	C_{FF} Chapter
5.0	55.36	10	4.7	100	22	22×2	C_{FF} Chapter

All the external components are the suggested values, the final values are based on the application testing results.

Selecting the Inductor

The recommended inductor values are shown in the table above. It is important to guarantee the inductor core does not saturate during any foreseeable situation. The inductor should be rated to handle the maximum inductor peak current: Care should be taken when reviewing the different saturation current ratings that are specified by different manufacturers. Saturation current ratings are typically specified at 25°C, so ratings at maximum ambient temperature of the application should be requested from the manufacturer. The inductor value can be calculated with:

$$L = \frac{V_{OUT} \times (V_{IN} - V_{OUT})}{V_{IN} \times \Delta I_L \times F_{OSC}}$$

Where ΔI_L is the inductor ripple current. Choose inductor ripple current to be approximately 30% to 50% of the maximum load current. The maximum inductor peak current can be estimated as:

$$I_{L(MAX)} = I_{LOAD} + \frac{\Delta I_L}{2}$$

Under light load conditions below 100mA, larger inductance is recommended for improved efficiency. Larger inductances lead to smaller ripple current and voltage, but they also have larger physical dimensions, lower saturation currents and higher linear impedance. Therefore, the choice of inductance should be compromised according to the specific application.

Selecting the Input Capacitor

The input current to the step-down converter is discontinuous and therefore requires a capacitor to supply the AC current while maintaining the DC input voltage. For a better performance, use ceramic capacitors placed as close to VIN as possible. A 0.1μF input capacitor to filter out high frequency interference is recommended. Capacitors with X5R and X7R ceramic dielectrics are recommended because they are stable with temperature fluctuations.

The capacitors must also have a ripple current rating greater than the maximum input ripple current of the converter. The input ripple current can be estimated with Equation:

$$I_{CIN} = I_{OUT} \times \sqrt{\frac{V_{OUT}}{V_{IN}} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right)}$$

From the above equation, it can be concluded that the input ripple current reaches its maximum at $V_{IN}=2V_{OUT}$ where $I_{CIN} = \frac{I_{OUT}}{2}$. For simplification, choose an input capacitor with an RMS current rating greater than half of the maximum load current.

The input capacitance value determines the input voltage ripple of the converter. If there is an input voltage ripple requirement in the system, choose the input capacitor that meets the specification. The input voltage ripple can be estimate with Equation:

$$\Delta V_{IN} = \frac{I_{OUT}}{F_{OSC} \times C_{IN}} \times \frac{V_{OUT}}{V_{IN}} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right)$$

Similarly, when $V_{IN}=2V_{OUT}$, input voltage ripple reaches its maximum of $\Delta V_{IN} = \frac{1}{4} \times \frac{I_{OUT}}{F_{OSC} \times C_{IN}}$.

Selecting the Output Capacitor

An output capacitor is required to maintain the DC output voltage. The output voltage ripple can be estimated with Equation:

$$\Delta V_{OUT} = \frac{V_{OUT}}{F_{OSC} \times L} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right) \times \left(R_{ESR} + \frac{1}{8 \times F_{OSC} \times C_{OUT}}\right)$$

There are some differences between different types of capacitors. In the case of ceramic capacitors, the impedance at the switching frequency is dominated by the capacitance. The output voltage ripple is mainly caused by the capacitance. For simplification, the output voltage ripple can be estimated with Equation:

$$\Delta V_{OUT} = \frac{V_{OUT}}{8 \times F_{OSC}^2 \times L \times C_{OUT}} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right)$$

A larger output capacitor can achieve a better load transient response, but the maximum output capacitor limitation should also be considered in the design application. If the output capacitor value is too high, the output voltage will not be able to reach the design value during the soft-start time and will fail to regulate. The maximum output capacitor value (COUT_MAX) can be limited approximately with Equation:

$$C_{OUT_MAX} = (I_{LIM_AVG} - I_{OUT}) \times T_{SS} / V_{OUT}$$

Where I_{LIM_AVG} is the average start-up current during the soft-start period, and T_{SS} is the soft- start time.

On the other hand, special attention should be paid when selecting these components. The DC bias of these capacitors can result in a capacitance value that falls below the minimum value given in the recommended capacitor specifications table.

The ceramic capacitor's actual capacitance can vary with temperature. The capacitor type X7R, which operates over a temperature range of -55°C to +125°C, will only vary the capacitance to within ±15%. The capacitor type X5R has a similar tolerance over a reduced temperature range of -55°C to +85°C. Many large value ceramic capacitors, larger than 1uF are manufactured with Z5U or Y5V temperature characteristics. Their capacitance can drop by more than 50% as the temperature varies from 25°C to 85°C. Therefore, X5R or X7R is recommended over Z5U and Y5V in applications where the ambient temperature will change significantly above or below 25°C.

Feed-Forward Capacitor (C_{FF})

SK6252B has internal loop compensation, so adding C_{FF} is optional. For specific applications, if necessary, consider whether to add feed-forward capacitors according to the situation.

The use of a feed-forward capacitor (C_{FF}) in the feedback network is to improve the transient response or higher phase margin. For optimizing the feed-forward capacitor, knowing the cross frequency is the first thing. The cross frequency (or the converter bandwidth) can be determined by using a network analyzer. When getting the cross frequency with no feed-forward capacitor identified, the value of feed-forward capacitor (C_{FF}) can be calculated with the following equation:

$$C_{FF} = \frac{1}{2\pi \times F_{CROSS}} \times \sqrt{\frac{1}{R1} \times \left(\frac{1}{R1} + \frac{1}{R2} \right)}$$

Where F_{CROSS} is the cross frequency.

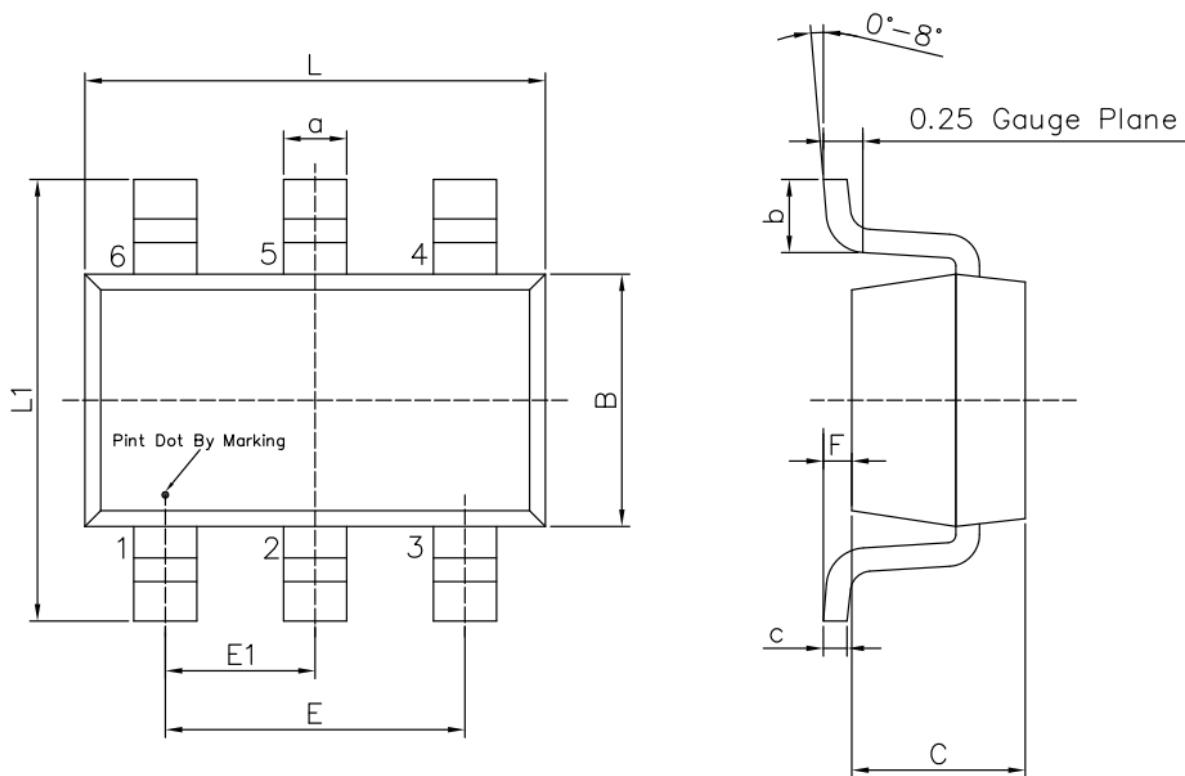
To reduce transient ripple, the feed-forward capacitor value can be increased to push the cross frequency to higher region. Although this can improve transient response, it also decreases phase margin and cause more ringing. In the other hand, if more phase margin is desired, the feed-forward capacitor value can be decreased to push the cross frequency to lower region.

PCB LAYOUT CONSIDERATION

PCB layout is very important to achieve stable operation and better performance. It is highly recommended to duplicate EVB layout for optimum performance. If change is necessary, please follow these guidelines for reference.

1. Keep the path of switching current short and minimize the loop area formed by Input capacitor, high-side MOSFET and low-side MOSFET.
2. Bypass ceramic capacitors are suggested to be put close to the VIN Pin.
3. Ensure all feedback connections are short and direct. Place the feedback resistors and compensation components as close to the chip as possible.
4. VOUT, SW away from sensitive analog areas such as FB.
5. Connect IN, SW, and especially GND respectively to a large copper area to cool the chip to improve thermal performance and long-term reliability.

PACKAGE DIMENSIONS: SOT23-6



Unit: mm

Symbol	Dimensions In Millimeters		Symbol	Dimensions In Millimeters	
	Min	Max		Min	Max
L	2.80	3.00	E1	0.85	1.05
B	1.50	1.70	a	0.30	0.50
C	0.90	1.30	c	0.09	0.20
L1	2.60	3.00	b	0.35	0.55
E	1.80	2.00	F	0	0.15

Note:

- 1) All dimensions are in millimeters.
- 2) Package length does not include mold flash, protrusion or gate burr.
- 3) Package width does not include inter lead flash or protrusion.
- 4) Lead popularity (bottom of leads after forming) shall be 0.10 millimeters max.
- 5) Pin 1 is lower left pin when reading top mark from left to right.